



# ***Effects of water ageing on the mechanical properties of flax and glass fibre composites: Degradation and reversibility***

**G. APOLINARIO TESTONI, P. IENNY, S. CORN, R. LEGER, A. BERGERET, J.M. HAUDIN**



Centre des Matériaux des Mines d'Alès (C2MA), Ecole des mines d'Alès, Alès, France

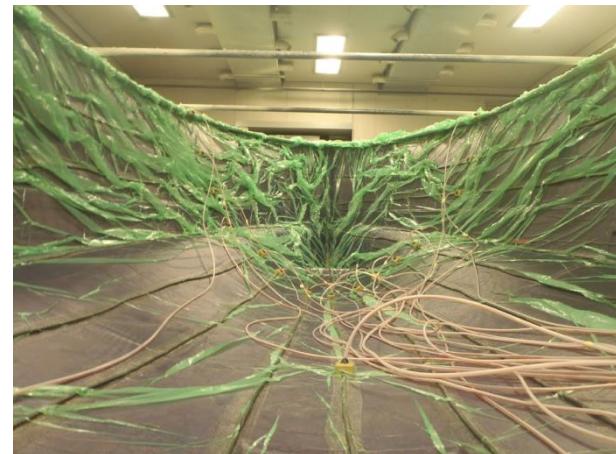
Centre de Mise en Forme des Matériaux (CEMEF), Mines ParisTech, Sophia-Antipolis, France

# Context of the presentation

- In France:

**20.000 boats reach their end-of-life in 2015**

**95% are manufactured with Glass-polyester composites.**



Ref.: Le Duigou et al. 2014 / French Nautical Industries Federation.

# Context of the presentation

**Societal context due to new environmental legislation**

Societal promotion to develop bio-based composites to conventional ones



**One of the alternatives**

Introduction of plant fibres to substitute glass fibres



**A scientific challenge**

How reducing the water sensitivity of plant based composites ?

**Objective of the present study**

**Understanding the long-term influence of water on diffusivity  
and mechanical property through modelling**

Refs.: Davies et al, 1996 ; Camino et al, 1997 ; Gellert et al, 1999 ; Pillin et al, 2011 ; Darshil et al, 2013 ; Faruk et al, 2012 ; Bledzki et Gassan, 1998 ; Scida et al, 2013 ; Le Duigou et al, 2009; Dhakal, 2007.

# Methodology of the study

Glass Fibre Reinforced Composites  
**GFRC**

Flax Fibre Reinforced Ccomposites  
**FFRC**

**Chemical treatment**  
Reduces their hydrophilicity

**Immersion into water**

Water uptake → Mechanical properties evolution

**Dessication**

Recovery of mechanical properties → Reversible / Irreversible degradation

**Predictive Modelling**



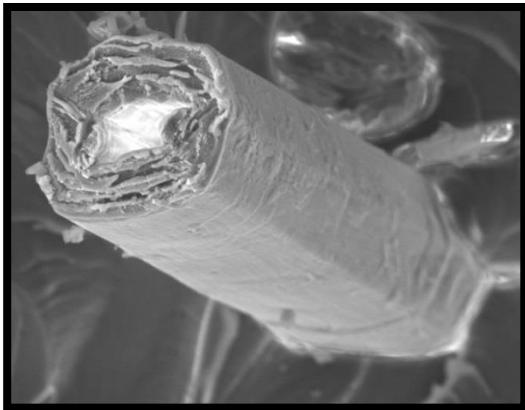
## SUMMARY

**Materials & Processing**

**Methods**

**Results & Discussion**

**Conclusions & Perspectives**



*Flax / Polyester composite  
MEB C2MA-Mines Alès (200X).*



# Materials & Methods

## Materials & Processing

Unsaturated polyester resin  
Glass & Flax fibres  
Chemical treatment  
Composites

## Methods

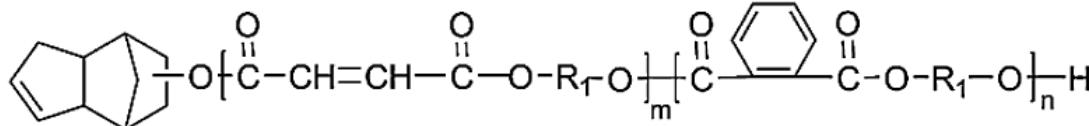
Water ageing  
Composites drying  
Viscoelastic properties  
Uniaxial tensile tests  
Differential Scanning calorimetry

# Materials

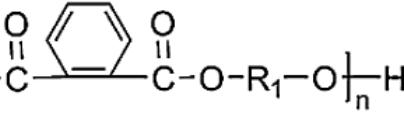
## Polyester resin

Dicyclopentadiene isophthalic unsaturated polyester resine

Enydyne® N50 1912 AI (Cray Valley)



**Catalyzer**  
1,8% MEKP



## Fibres

Unidirectionnal fibres



Glass fibres



Flax fibres

Grammage supplier database:

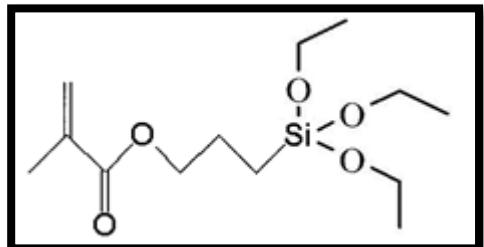
Cross-linked resin (supplier datasheet)	
Properties	Values
Density	1,17 g/cm3
Glass transition temperature	57-60 °C
Degradation temperature	230-250°C
Flexural ISO 178	
Young Modulus	3000 MPa
Maximum strength	70 MPa

# Materials

## ■ Chemical treatment

### Silane treatment

$\gamma$ -methacryloxypropyltrimethoxysilane (MPS)



MPS

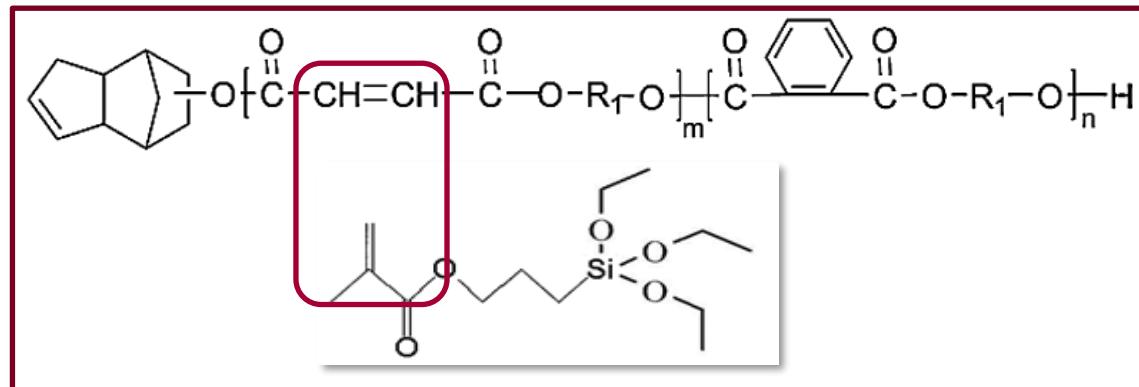
Methacrylate-function can display **good reactivity** with unsaturated polyester matrix.

### Experimental protocol:

- Solvent water/Ethanol (60/40 wt.%)
- 1.0 wt.% compared to flax fibres
- Hydrolyse : 3h
- acid pH 4
- Drying oven 105°C / 2h

Ref. : Xie et al., 2010

**Fibre impregnation:**  
Padding bath with the  
finishing solution.

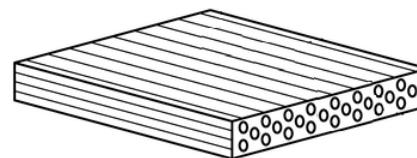
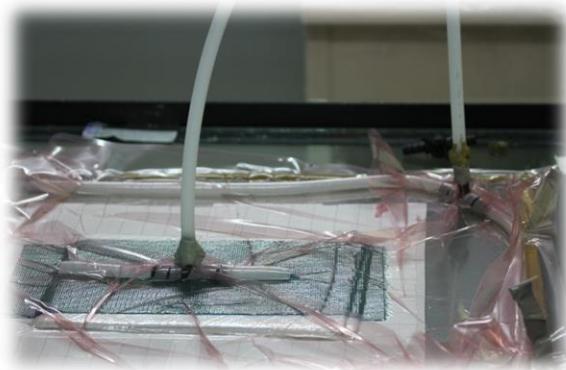


Silane treatment aims to create a **hydrophobic fibre surface**.

# Materials

## ■ Composites

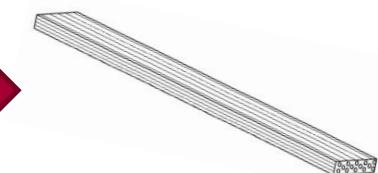
### Vacuum infusion processing of composite sheets



Composite  
sheets



Diamond  
cutter



Samples  
(250 x 25 mm<sup>2</sup>)

Vaccum pressure: 100 mBar

Conditions : 23°C / 50% h.r.

**Post cure:**

60°C / 24h

Resin crosslinking rate after  
postcuring : 88%

Composites	Layers	Thickness	Fibre content
	Units	(mm)	(%)
Glass FRC	6	1.8 – 2.1	52 – 56
Flax FRC	4	2.7 – 3.4	29 – 35

# Methods

## ■ Water ageing

- Time, temperature
  - More than 6 months at 30°C

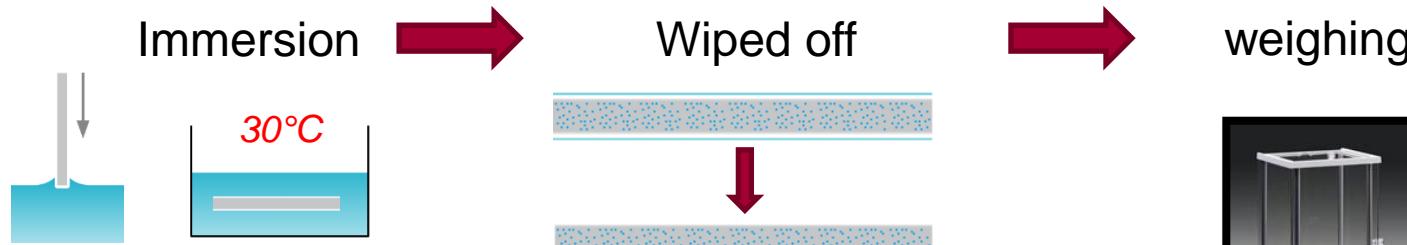
Julabo Thermostat  
(serpentine system)  
Temperature: 20 to 150°C



## ■ Physico chemical characterisation

- Sorption / desorption

### Sorption measurements

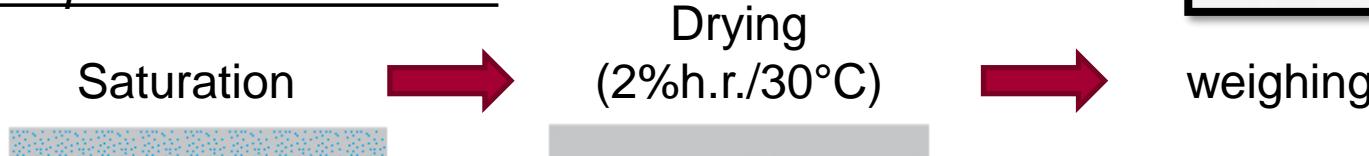


Water content variations:

$$W(\%) = ((W_t - W_o)/W_o) \times 100$$

Balance  
Mettler-Toledo AT200.  
**Precision: 0.1 mg**

### Desorption measurements

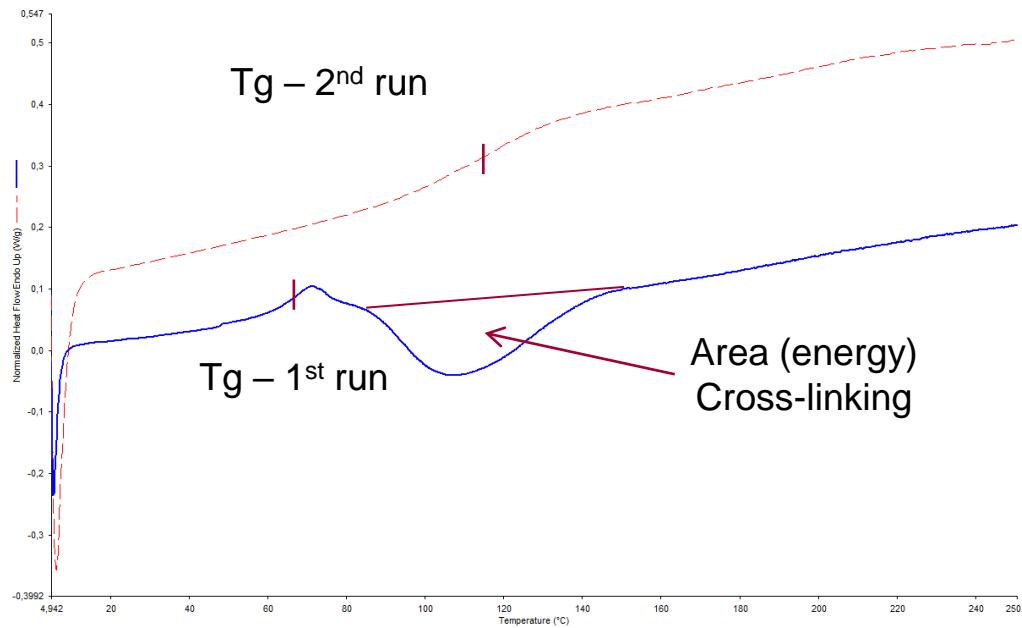


# Methods

## ■ Physico-chemical characterization

### Differential scanning calorimetry

- Crosslinking rate
- Glass transition temperature ( $T_g$ )



# Methods

## ■ Mechanical characterization

Static tensile testing

E  
 $\sigma$  rupture  
 $\varepsilon$  rupture

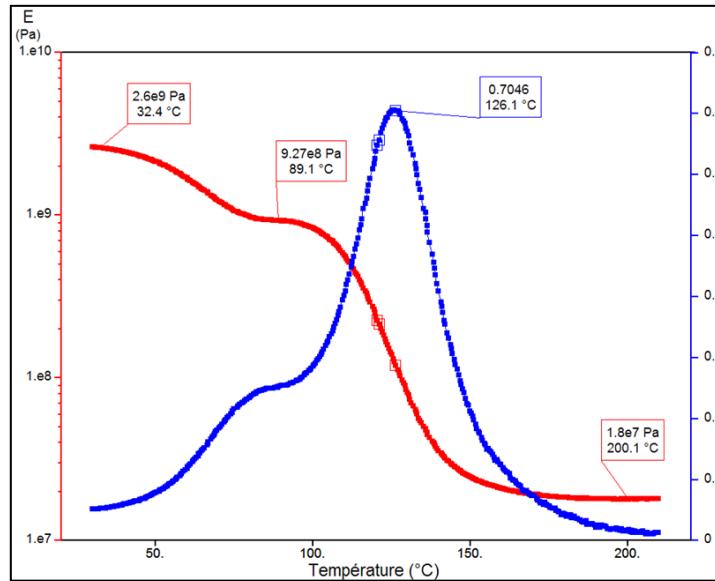


# Methods

## ■ Mechanical characterization

Dynamic tensile testing  
(DMA)

$E' (T,\omega)$   
 $\eta (T,\omega)$   
 $T_a$

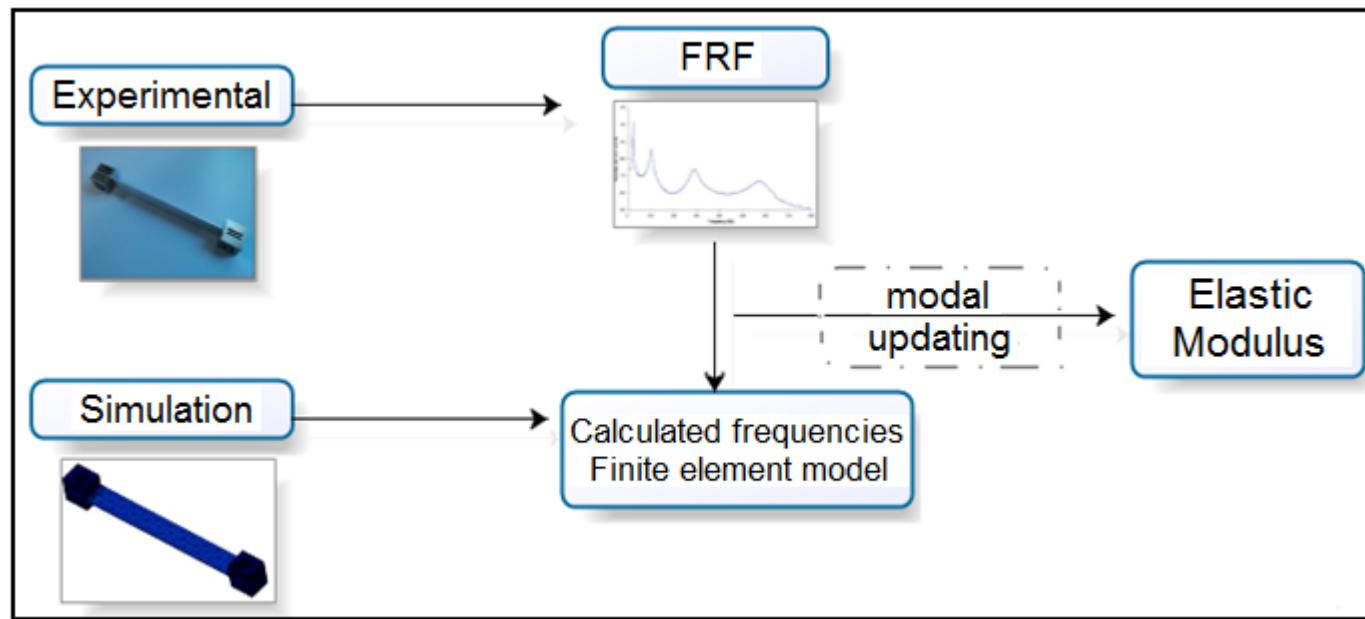


# Methods

## ■ Mechanical characterization

Free vibration analysis  
(Non-destructive test)

$$\begin{cases} E'(\omega_i) \\ \eta'(\omega_i) \end{cases}$$





# Results and discussion

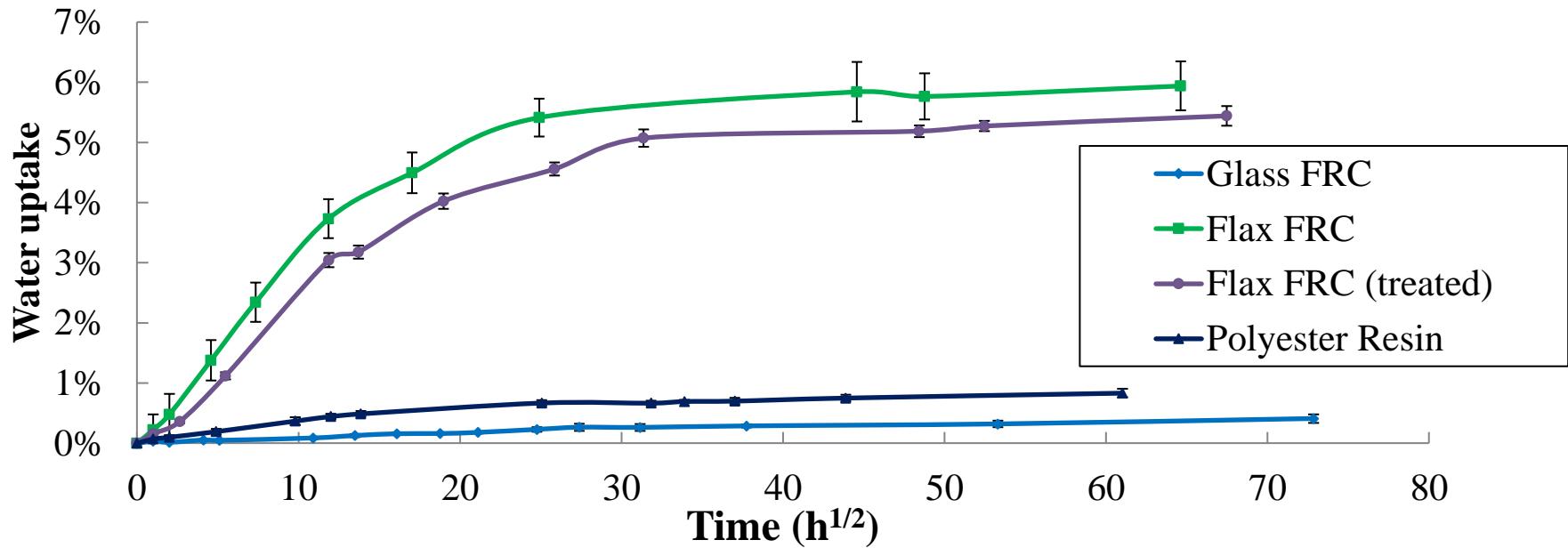
Hydroscopic properties

Mechanical properties

Reversibility

# Results and discussion

## Hydroscopic properties



Materials	<i>Experimental data</i>	
	Diffusivity ( $m^2/s$ )	Saturation (%)
Polyester resin	$4.6 \times 10^{-6}$	0.9
Glass FRC	$1.2 \times 10^{-7}$	0.4
Flax FRC	$5.4 \times 10^{-6}$	5.9
Flax FRC (treated)	$4.3 \times 10^{-6}$	5.3

Identification: Fick's Law 1D

Fibres	Saturation (%)
Glass fibres	- 0,21
Flax fibres	+ 16,4

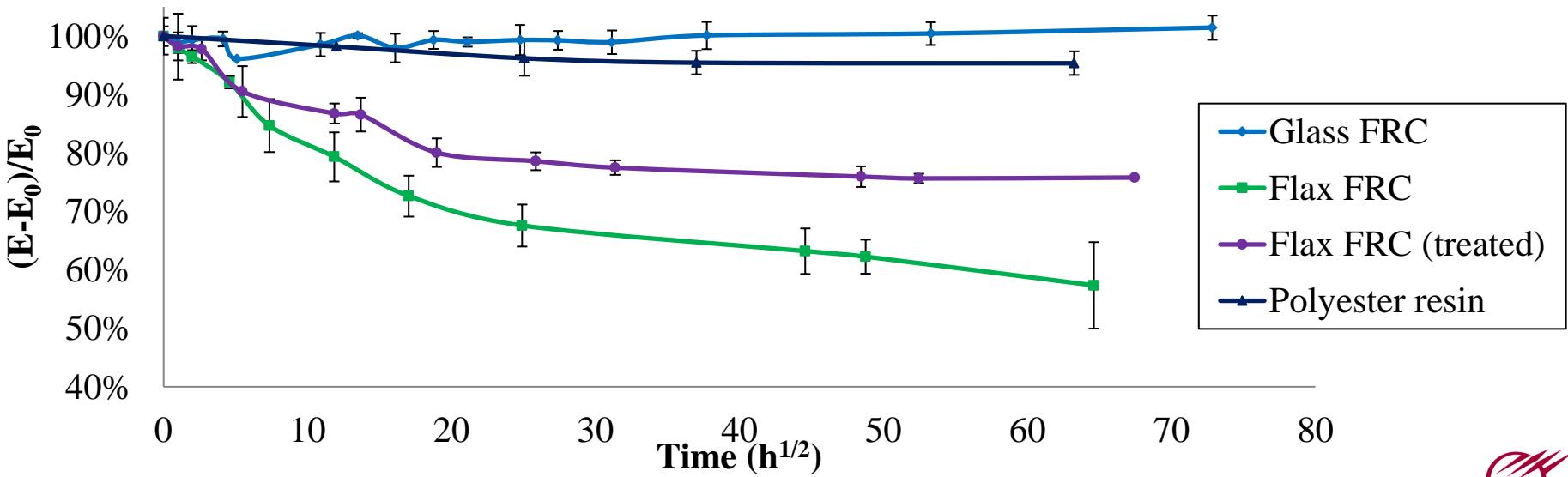
Rule of mixtures (inversed method)

# Results and discussion

## Mechanical properties

- Relative modulus evolution (vibration analysis)

Materials	Initial $E_0$ (GPa)	Modulus evolution $E_{\text{sat}}/E_0$
Polyester resin	$3.25 \pm 0.64$	-5%
GFRC	$34.88 \pm 1.16$	0%
FFRC	$20.26 \pm 1.16$	-37%
FFRC (treated)	$20.44 \pm 0.74$	-22%

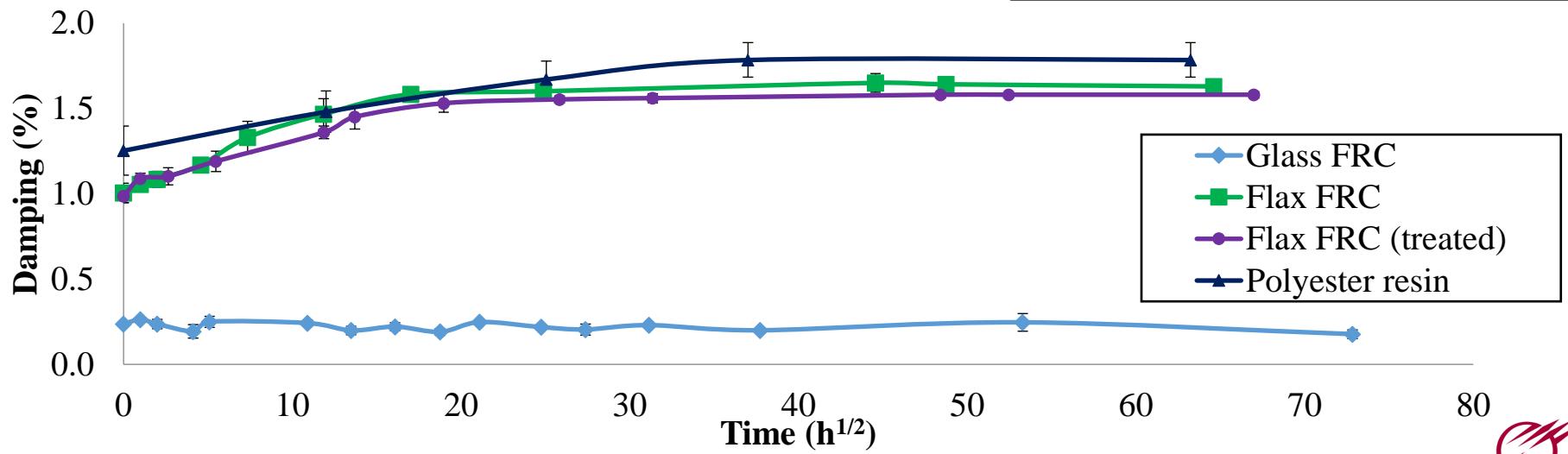
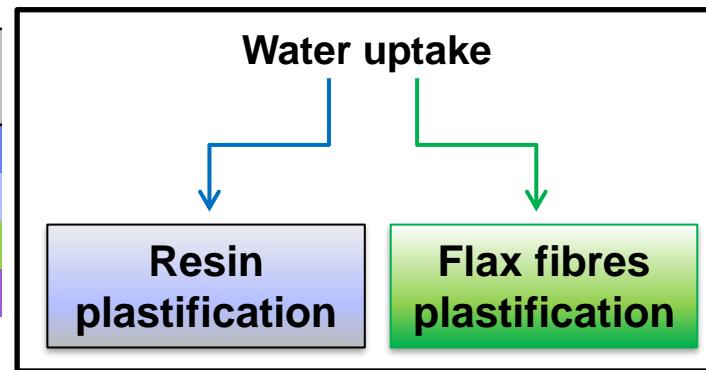


# Results and discussion

## Mechanical properties

- Damping evolution (vibration analysis)

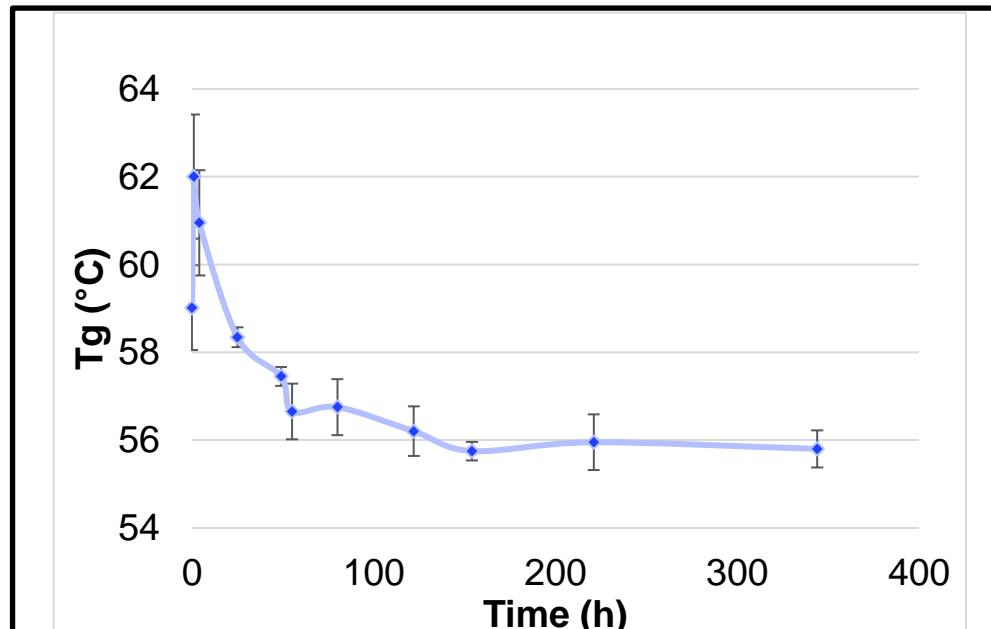
Materials	Initial $a_0$ (%)	Damping evolution $a_{\text{sat}}/a_0$
Polyester resin	$1.25 \pm 0.18$	+42%
GFRC	$0.24 \pm 0.01$	-8%
FFRC	$1.00 \pm 0.06$	+62%
FFRC (treated)	$0.99 \pm 0.04$	+57%



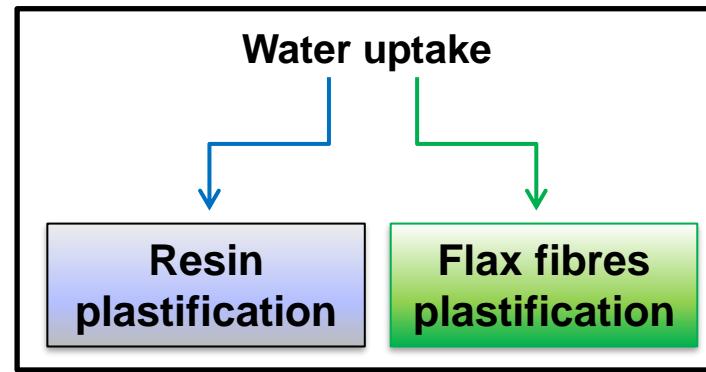
# Results and discussion

## Mechanical properties

- Damping evolution (vibration analysis)



**Resin plastification**  
(reduction in Tg)

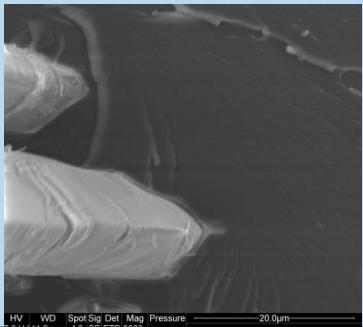


# Results and discussion

## Mechanical properties

- Fracture surface analysis of Flax FRC (ESEM)

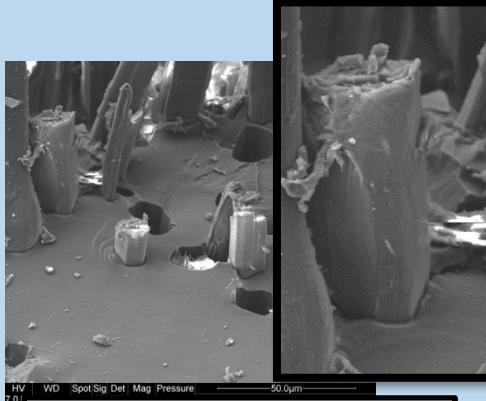
Before immersion



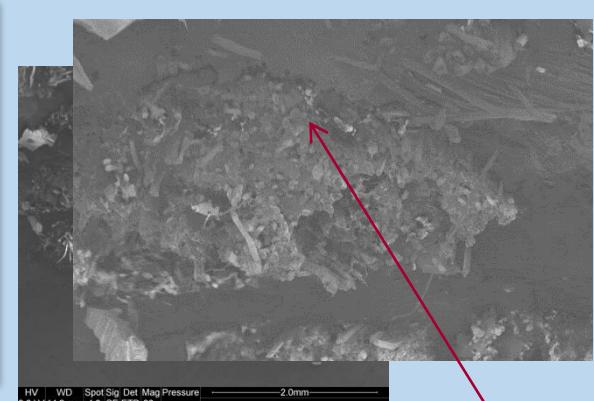
Interfacial cohesion



Fibres  
« Peeling »

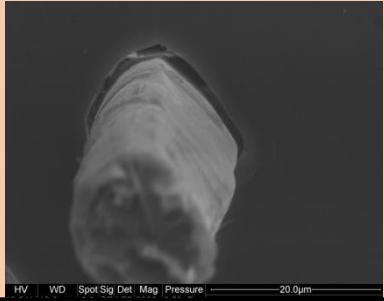


Fibres sharp break



Revelling length

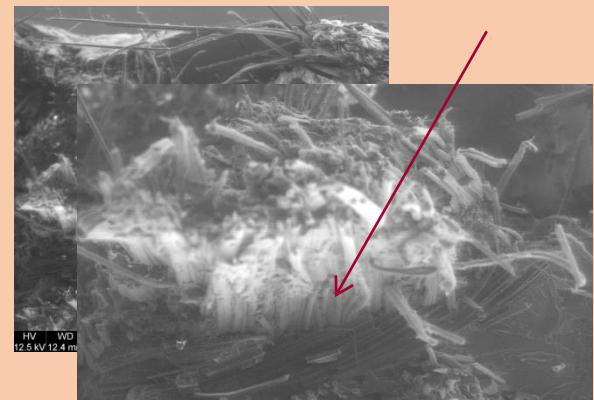
After immersion



Surface debonding



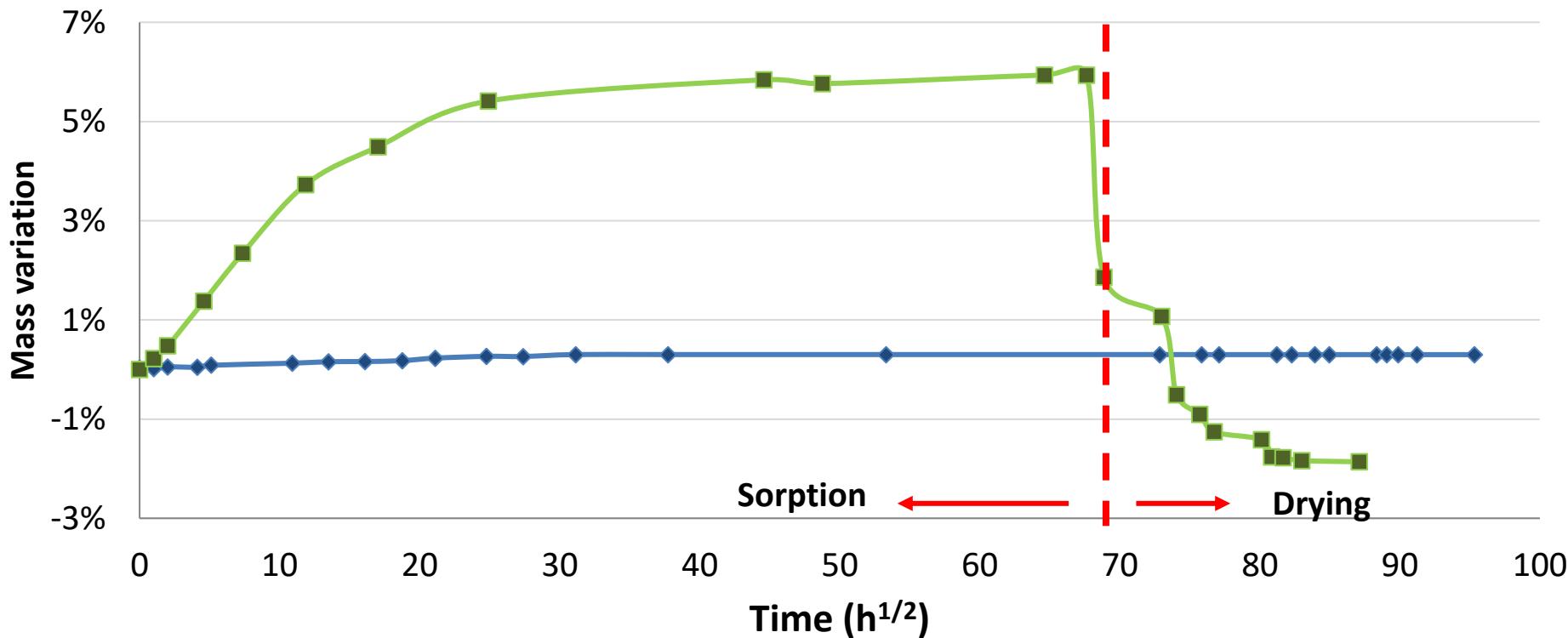
Fibre plasticization



# Results and discussion

## ■ Reversibility

Sorption : Immersion at 30°C  
Drying: 2% h.r. / 30°C

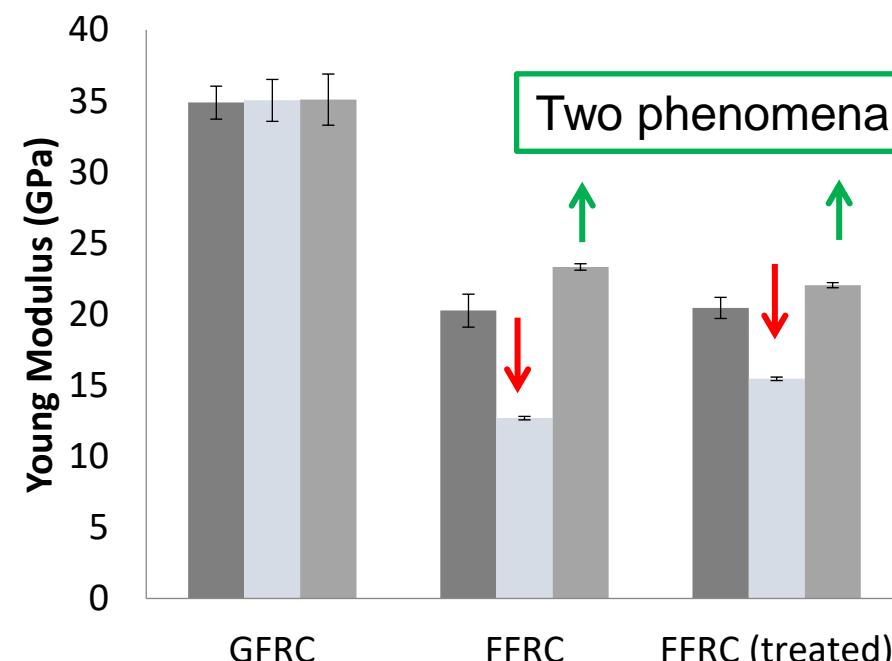


# Results and discussion

## ■ Reversibility

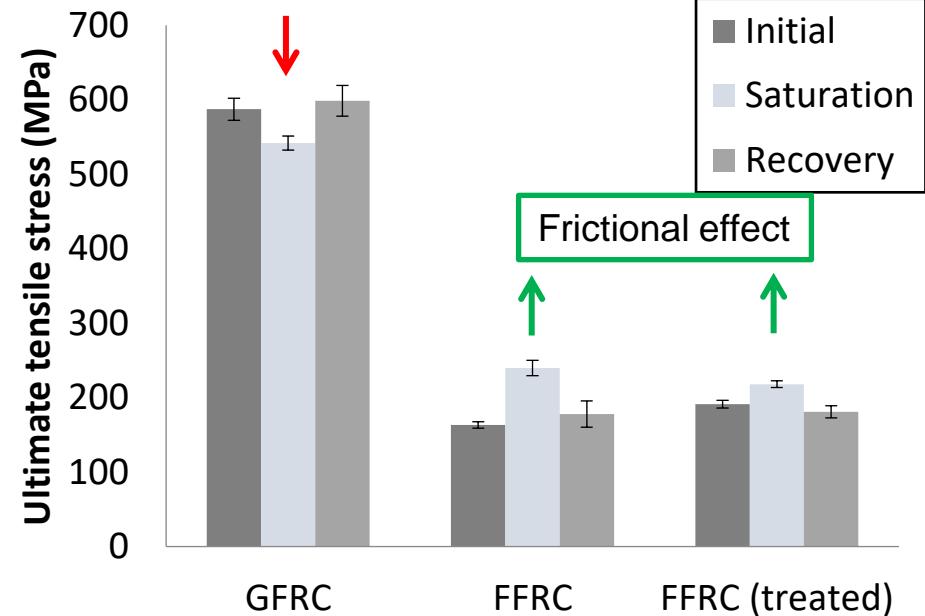
Sorption : Immersion at 30°C  
Drying: 2% h.r. / 30°C

GFRC are not affected



Two phenomena

Interfacial debonding



Frictional effect

# Results and discussion

## ■ Reversibility

Materials	Initial E (GPa)	Reversibility E (GPa)
CRFV	$34.88 \pm 1.16$	$35.09 \pm 1.79$
CRFL	$20.26 \pm 1.16$	$23.32 \pm 0.22$   <b>13%</b>

### Rule of mixtures

$$E_c = V_f E_f + V_m E_m \rightarrow E_c \uparrow \text{ 13%} \quad \rightarrow \quad E_m \uparrow \text{ 21%} \quad -\text{Crosslinking}$$

### Hypotheses

**Evolution of the matrix crosslinking rate throughout water ageing period.**

# Results and discussion

## ■ Reversibility

### Hypotheses

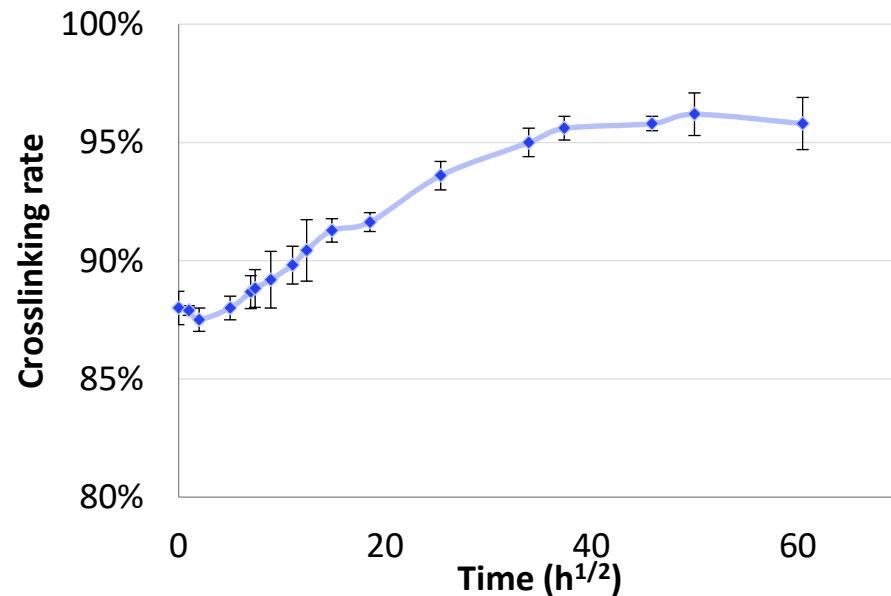
**Evolution of the matrix crosslinking rate** throughout water ageing period.

### **DSC characterization:**

Cross-linking conditions:

Cure - 24h at room temperature

Post-cure - 16h at 40°C



Polyester resin	E - 30°C(MPa)	Tan delta (30°C)
Before immersion	$2827 \pm 165$	$0,044 \pm 0,005$
After drying	$3434 \pm 71$	$0,026 \pm 0,002$

# Results and discussion

## ■ Reversibility

Materials	Initial E (GPa)	Reversibility E (GPa)
CRFV	$34.88 \pm 1.16$	$35.09 \pm 1.79$
CRFL	$20.26 \pm 1.16$	$23.32 \pm 0.22$   <b>13%</b>

### Rule of mixtures

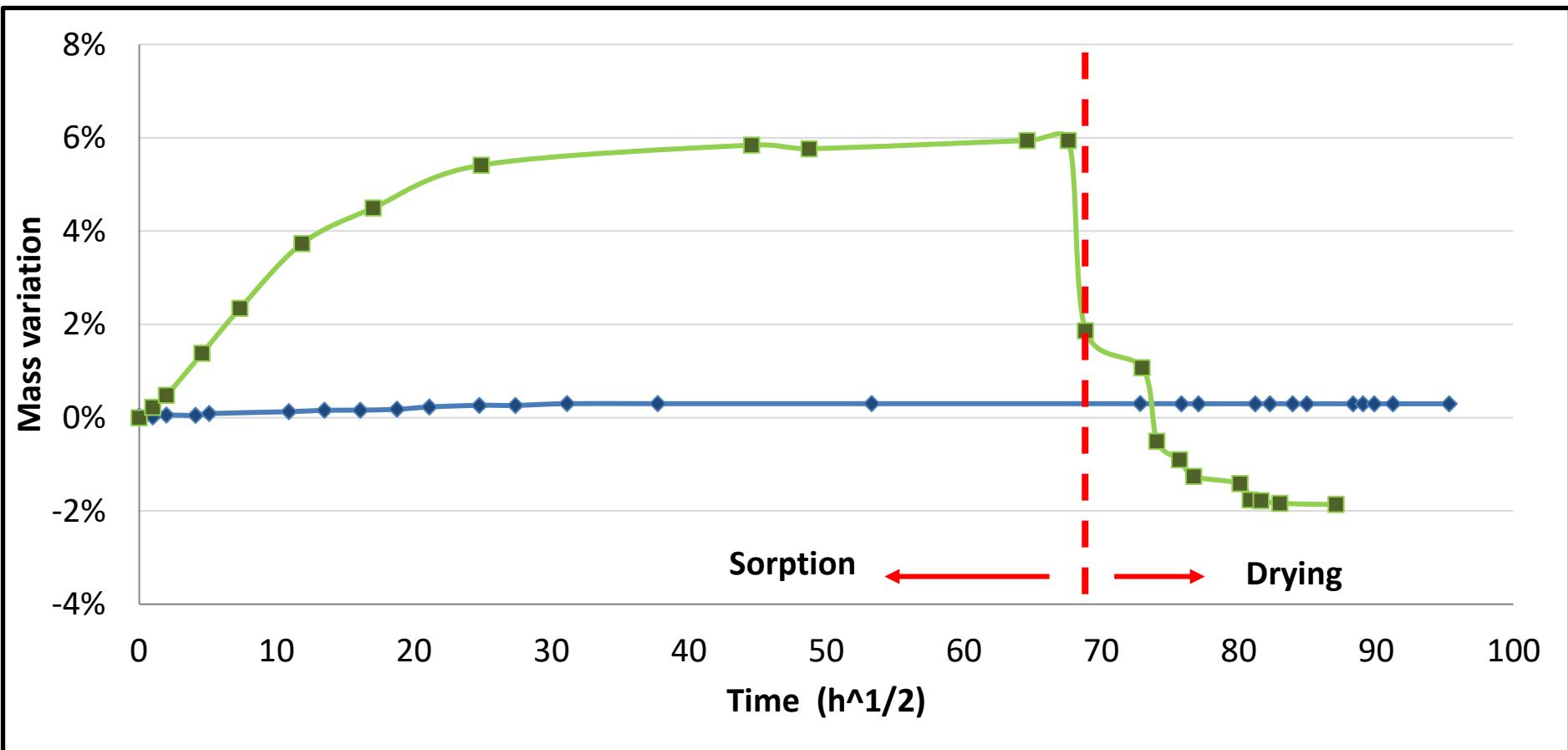
$$E_c = V_f E_f + V_m E_m \rightarrow E_c \uparrow \text{ } \underline{13\%}$$

  $E_m$   **21%** -Crosslinking

  $E_f$   **17%** - Fibres drying

# Results and discussion

## ■ Reversibility



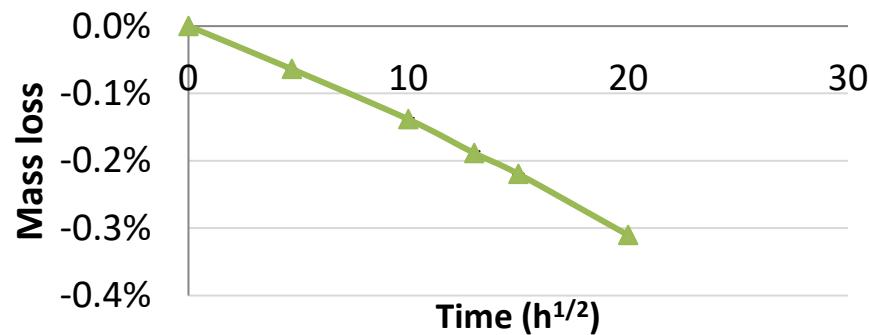
# Results and discussion

## ■ Reversibility

Flax FRC reach a dried mass 2% lower than initial state before immersion:

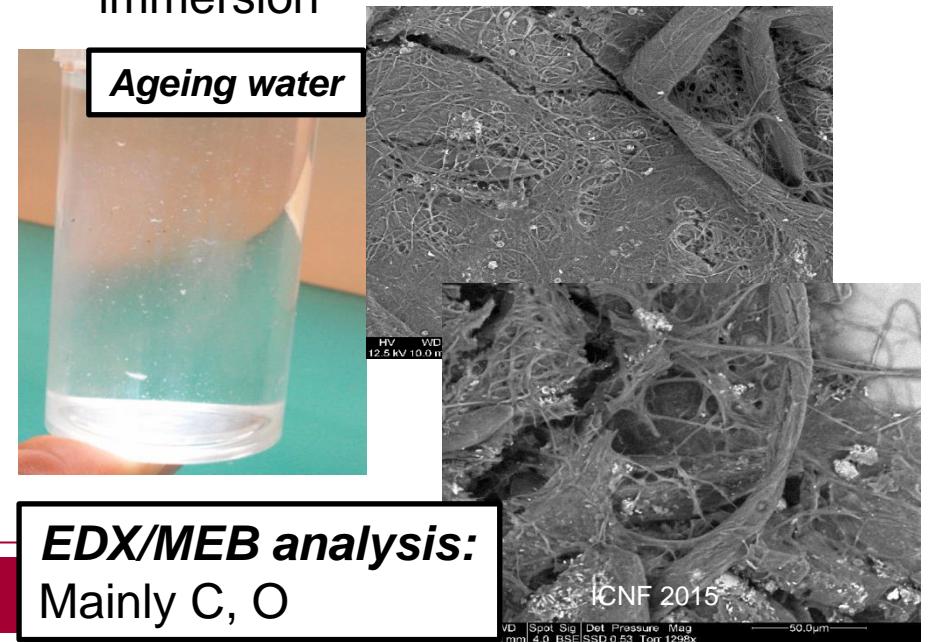
The weight loss after desiccation could be explained by two factors:

- The **fibres get drier** than at the initial state;



0,3% of total loss weight

- The **extractibles** (small cell-walls components) **were removed** during immersion



# Modelling

## ■ Hydro-thermal ageing modelling

- A Realistic predictive model take into account :



*Physico-chemical  
phenomena  
(only reversible)*

Diffusion

Fick's law

$c$  : Water concentration  
 $D$  : Diffusivity coefficient

Swelling

Hydric swelling  
Thermic swelling

$\rightarrow k$  : swelling coefficient

Plastification

Linear-elastic  
behaviour

$\rightarrow [C]$  : rigidity matrix

# Modelling

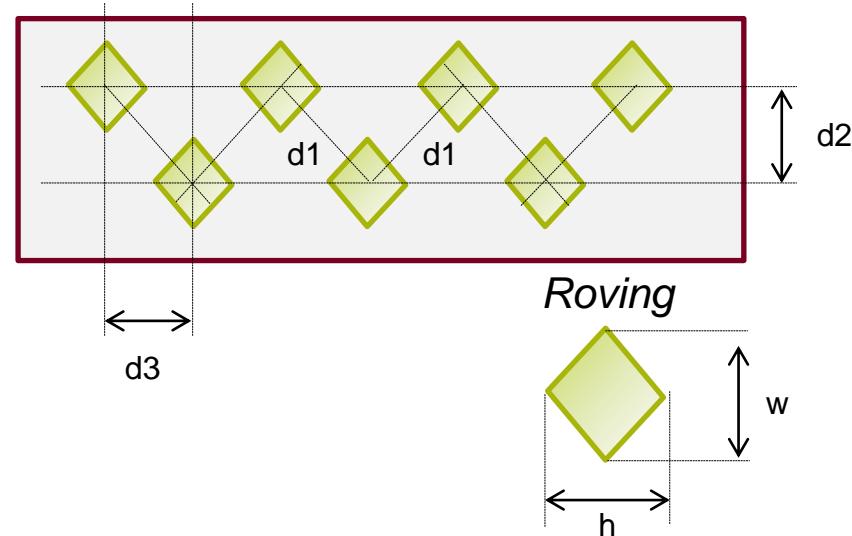
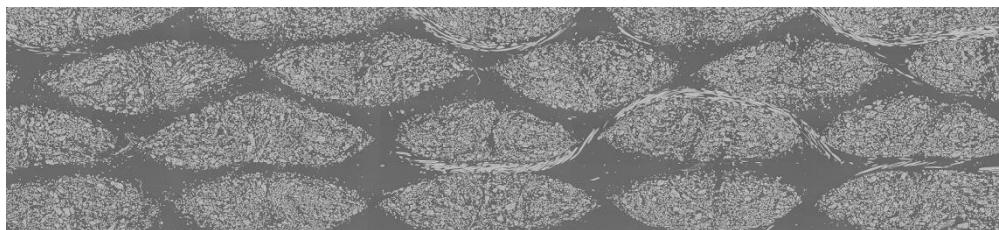
## ■ Multiphysics modelling

To obtain a realistic predictive model:

Complex multiscale composite morphology:

Statistics of roving parameters (size and distribution measurements);

Statistics of fibres / bundles (surface area, form factor, inter-particle distance).



# Modelling

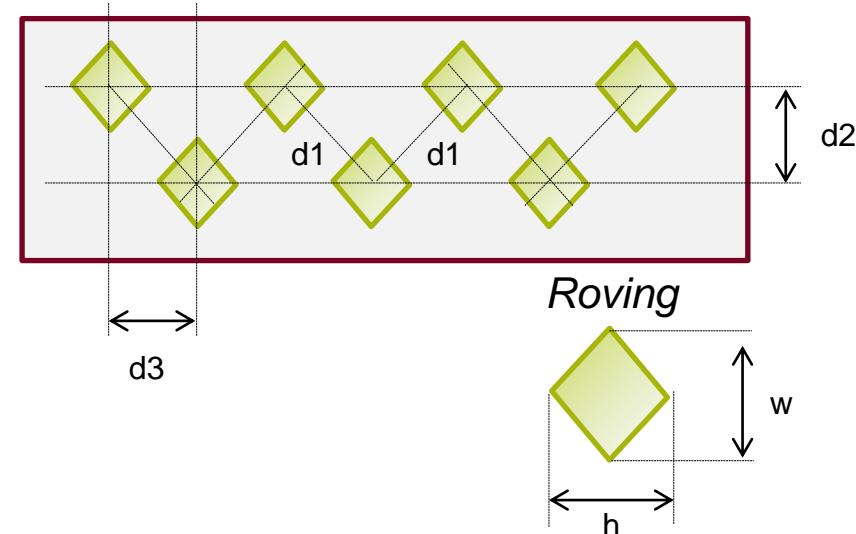
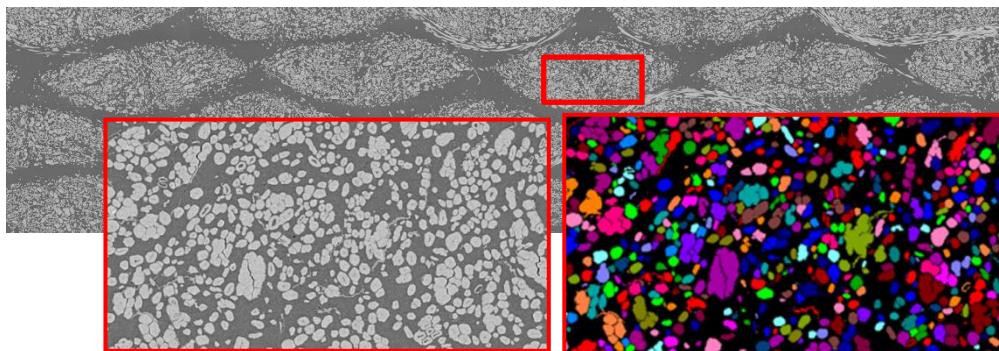
## Multiphysics modelling

To obtain a realistic predictive model:

Complex multiscale composite morphology:

Statistics of roving parameters (size and distribution measurements);

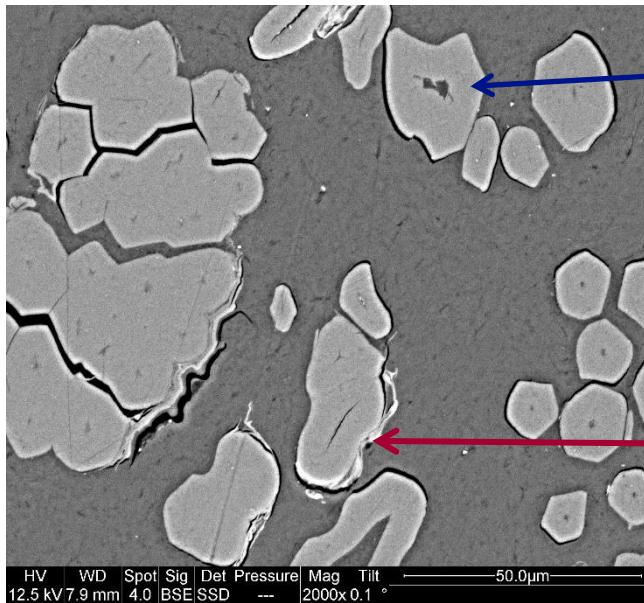
Statistics of fibres / bundles (surface area, form factor, inter-particle distance).



# Modelling

## ■ Multiphysics modelling

Influence of processing conditions on composite morphology:



**Matrix inside  
the lumen**

**Lumen flattened  
during vacuum infusion**

### The evolution of fibre and matrix behaviour (irreversible):

Matrix hardening  
Fibres extractibles removing

# Conclusions

## ■ The composites water uptake is mainly controlled by natural fibres.

- Composites rigidity decreases while damping increases;
- Ultimate properties increases at saturation.



Fibres  
plastification



Frictional effect caused  
by fibres swelling

## ■ Reversible ageing occurs during immersion at 30°C but:

- Further crosslinking is observed;
- Dried composites mass 2% lower than initial state before immersion



The loss weight is explained by drying the fibres initial humidity and by the removing of small cell-walls components removed during immersion.

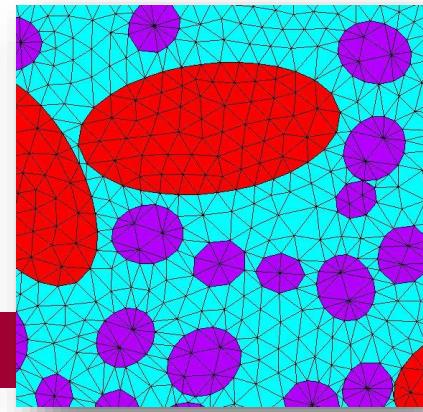
## ■ Define fibres distribution in composites after processing



Modeling

## Perspectives

- Modeling should take into account both **fibres swelling** and the **influence of processing** conditions on composite morphology;
- To mimic real in-service conditions, **thermo-hydro-mechanical ageing** tests will be investigated on studied materials.



A wide-angle photograph of a lush, green landscape. In the center, a large, deep blue lake is surrounded by dense green forests. A paved road winds its way around the lake and through the surrounding fields. In the background, a town is nestled in a valley, and a range of mountains rises under a clear sky.

Thank you