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# A Mathematical Framework for IMU Error Propagation with Applications to Preintegration

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#### Abstract

To fuse information from inertial measurement units (IMU) with other sensors one needs an accurate model for IMU error propagation in terms of position, velocity and orientation, a triplet we call extended pose. In this paper we leverage a nontrivial result, namely log-linearity of inertial navigation equations based on the recently introduced Lie group  $SE_2(3)$ , to transpose the recent methodology of Barfoot and Furgale for associating uncertainty with poses (position, orientation) of SE(3) when using noisy wheel speeds, to the case of extended poses (position, velocity, orientation) of  $SE_2(3)$  when using noisy IMUs. Besides, our approach to extended poses combined with loglinearity property allows revisiting the theory of preintegration on manifolds and reaching a further theoretic level in this field. We show exact preintegration formulas that account for rotating earth, that is, centrifugal force and Coriolis effect, may be derived as a byproduct.

## 1 Introduction

Geometric approaches to associating uncertainty with poses, essentially for mobile robot localization, have been largely successful in the robotics community over the past decade. Since the discovery that mobile robots dispersion under the effect of sensor noise resembles more a "banana" than a standard Gaussian ellipse, which can be traced back to [28], studies have evidenced the fact that the Lie group structure of the configuration space SE(3) plays a prominent role in probabilistic robotics, see [1, 12, 2, 29, 14, 3, 20, 26]. In particular, Gaussian distributions in

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(Lie) exponential coordinates provide accurate approximations of banana distributions as first advocated by [24]. The reader is also referred to the recent monographs [11, 1].

When inertial sensors (gyrometers and accelerometers) embedded in an Inertial Measurement Unit (IMU) are utilized, one needs to manipulate extended poses, which are 9 dimensional elements that cannot be modeled as elements of SE(3). Moreover, the IMU propagation equations are not amenable to left multiplications on Lie groups of the form  $\mathbf{T}_{k+1} = \mathbf{T}_k \mathbf{\Gamma}_k$ . This has had two consequences. First the results about uncertainty propagation of [2] are not easily transposed in an IMU context. Then, note that if IMU propagation equations were of the form above we would readily have  $\mathbf{T}_{k+N} = \mathbf{T}_k(\Pi_k^{N-1}\mathbf{\Gamma}_i)$ , and preintegrating IMU measurements as in [16] would be trivial, which is not the case. As a result, the theory of preintegration on manifolds [16] is more subtle and relies on smart algebraic tricks.

The recent introduction of group  $SE_2(3)$  along with the discovery of groupaffine property and hence log-linearity of IMU equations using  $SE_2(3)$  in [4, 5] proves a major step to overcome these obstacles. It has already led to more robust EKFs for fusion of IMU with other sensors, has prompted an industrial product, see [6], has improved EKF-based visual inertial consistency [30, 18, 9, 10, 19] and robot state estimation [17]. In this paper, we show the properties of  $SE_2(3)$  allow transposing the recent results about estimation of poses using wheel speeds of [2] to the context of IMUs. More precisely, our main contributions are as follows:

- We provide a nontrival extension of the approach and results of [2] which deals with position and orientation (i.e. pose) for odometry based robotics, to position, orientation plus velocity (i.e. extended pose) when using IMUs, leveraging the log-linear property of IMU equations of [5]. In particular we recover the banana shape characteristic of odometry based dispersion [24, 11, 1, 12, 2] in the context of IMU based navigation;
- We leverage log-linearity to provide a novel theoretic framework for preintegration on manifolds [16], extending preliminary results of [7] regarding bias and noise free IMU equations;
- Using a nontrivial trick, see eq. (13), we prove preintegration on rotating earth accounting for Coriolis effect and centrifugal forces may be achieved, and this thanks to our mathematical framework.

Secondary contributions as follows. First we redemonstrate the log-linear property of IMU equations [5] in discrete time using elementary computations. Then, regarding preintegration we come up with a novel first order development with respect to noise and bias based on Lie exponential coordinates that proves more accurate than the classical Taylor expansion of [16]. We derive additional exact preintegration formulas when IMU are either noise free, or bias free.

#### 1.1 Paper organization

Section 2 is a summary of our preliminary results about noise and bias free preintegration recently published in [7]. Section 3 proves the unexpected and novel result that IMU based navigation equations where earth rotation is taken into account have the log-linearity property, and hence allow derivation of IMU preintegration formulas in this context. Section 4 presents our theory for associating uncertainty with extended poses, with applications to IMU noise propagation. Finally Section 5 deals with IMU biases.

## 2 A matrix lie Group approach to IMU preintegration

We suggest the reader first familiarize with classical Lie groups of robotics, referring to [2] and ideally to [1, 11].

## **2.1** Mathematical Preliminary: the Group $SE_2(3)$

The special orthogonal group SO(3) that encodes orientation **R** of a rigid body in space may be modeled as:

$$SO(3) := \{ \mathbf{R} \in \mathbb{R}^{3 \times 3} \mid \mathbf{R}^T \mathbf{R} = I_3, \text{ det } \mathbf{R} = 1 \}.$$

In turn, the set of poses, i.e., position  $\mathbf{X}$  and orientation  $\mathbf{R}$ , may be modeled using the matrix representation of the special Euclidean group

$$SE(3) := \{ \mathbf{T} = \begin{pmatrix} \mathbf{R} & \mathbf{X} \\ \mathbf{0}_{1,2} & 1 \end{pmatrix} \in \mathbb{R}^{4 \times 4} \mid (\mathbf{R}, \mathbf{X}) \in SO(3) \times \mathbb{R}^3 \}.$$

Finally to describe *extended poses*, i.e. position  $\mathbf{X}$ , velocity  $\mathbf{V}$  and orientation  $\mathbf{R}$ , we introduced the following group

$$SE_2(3) := \{ \mathbf{T} = \begin{pmatrix} \mathbf{R} & \mathbf{V} & \mathbf{X} \\ 0_{1,3} & 1 & 0 \\ 0_{1,3} & 0 & 1 \end{pmatrix} \mid (\mathbf{R}, \mathbf{V}, \mathbf{X}) \in SO(3) \times \mathbb{R}^3 \},$$

in [5] (see also [4]) we called group of "double direct spatial isometries". The latter are all matrix Lie groups, embedded in respectively  $\mathbb{R}^{3\times3}$ ,  $\mathbb{R}^{4\times4}$ , and  $\mathbb{R}^{5\times5}$ . Matrix multiplication then provides group composition of two elements of  $SE_2(3)$ . We see

the obtained composition is a natural extension of poses composition as elementary computations show  $(\mathbf{R}_1, \mathbf{V}_1, \mathbf{X}_1) \cdot (\mathbf{R}_2, \mathbf{V}_2, \mathbf{X}_2) = (\mathbf{R}_1 \mathbf{R}_2, \mathbf{R}_1 \mathbf{V}_2 + \mathbf{V}_1, \mathbf{R}_1 \mathbf{X}_2 + \mathbf{X}_1).$ 

As in classical Lie group theory, small perturbations of extended poses may be described by elements of the Lie algebra  $\mathfrak{se}_2(3)$ . The operator  $\wedge$  turns elements  $\boldsymbol{\xi} := (\boldsymbol{\omega}^T, \mathbf{v}^T, \mathbf{x}^T)^T \in \mathbb{R}^9$  into elements of the Lie algebra:

$$\boldsymbol{\xi}^{\wedge} := \begin{pmatrix} \boldsymbol{\omega} \\ \mathbf{v} \\ \mathbf{x} \end{pmatrix}^{\wedge} = \begin{pmatrix} (\boldsymbol{\omega})_{\times} & \mathbf{v} & \mathbf{x} \\ \mathbf{0}_{1,3} & \mathbf{0} & \mathbf{0} \\ \mathbf{0}_{1,3} & \mathbf{0} & \mathbf{0} \end{pmatrix}$$

where  $(\omega)_{\times} \in \mathbb{R}^{3\times 3}$  denotes the skew symmetric matrix associated with cross product with  $\omega \in \mathbb{R}^3$ . The exponential map conveniently maps small perturbations encoded in  $\mathbb{R}^9$  to  $SE_2(3)$ . For matrix Lie groups it is defined as

$$\exp(\boldsymbol{\xi}) := \exp_m(\boldsymbol{\xi}^{\wedge}),$$

where  $exp_m$  denotes the classical matrix exponential. The following closed form expression may be shown [5, 4]:

$$\exp\begin{pmatrix} \boldsymbol{\omega} \\ \mathbf{v} \\ \mathbf{x} \end{pmatrix} = \begin{pmatrix} \exp_m((\boldsymbol{\omega})_{\times}) & N(\boldsymbol{\omega})\mathbf{v} & N(\boldsymbol{\omega})\mathbf{x} \\ 0_{1,3} & 1 & 0 \\ 0_{1,3} & 0 & 1 \end{pmatrix}$$
(1)

with  $N(\omega) = I_3 + \frac{1 - \cos(||\omega||)}{||\omega||^2})((\omega)_{\times})^2 + \frac{||\omega|| - \sin(||\omega||)}{||\omega||^3}((\omega)_{\times})^3$ . The Baker-Campbell-Hausdorff (BCH) formula stipulates that for  $\boldsymbol{\xi}_1, \boldsymbol{\xi}_2 \in \mathbb{R}^9$  we have  $\exp(\boldsymbol{\xi}_1) \exp(\boldsymbol{\xi}_2) \approx \exp(\boldsymbol{\xi}_1 + \boldsymbol{\xi}_2)$  up to second order terms in  $\boldsymbol{\xi}_1, \boldsymbol{\xi}_2$ . Finally, the so-called adjoint operator is defined by analogy to SE(3) as:

$$Ad_{\mathbf{T}} = \begin{pmatrix} \mathbf{R} & \mathbf{0}_{3,3} & \mathbf{0}_{3,3} \\ (\mathbf{V})_{\times} \mathbf{R} & \mathbf{R} & \mathbf{0}_{3,3} \\ (\mathbf{X})_{\times} \mathbf{R} & \mathbf{0}_{3,3} & \mathbf{R} \end{pmatrix} \in \mathbb{R}^{9 \times 9},$$
(2)

where we conveniently describe it as an operator acting directly on  $\mathbb{R}^9$  instead of on the Lie algebra  $\mathfrak{se}_2(3)$ . We have the useful relation that can be considered as a definition:

$$\mathbf{T}\exp(\boldsymbol{\xi})\mathbf{T}^{-1} = \exp(Ad_{\mathbf{T}}\boldsymbol{\xi}). \tag{3}$$

#### 2.2 IMU Equations Revisited

We now summarize recent results [7]. Let  $\mathbf{R}_t$  denote the rotation matrix encoding the orientation of the IMU, and let  $\mathbf{X}_t$  and  $\mathbf{V}_t$  denote position and velocity of the

IMU. Let  $\mathbf{a}_t$  denote the specific acceleration, that is, true acceleration minus gravity vector  $\mathbf{g}$  expressed in the body frame, and  $\omega_t$  the angular velocity expressed in the body frame. The dynamical motion equations on flat earth write (see e.g. [16]):

$$\frac{d}{dt}\mathbf{R}_t = \mathbf{R}_t(\boldsymbol{\omega})_{\times}, \quad \frac{d}{dt}\mathbf{V}_t = \mathbf{g} + \mathbf{R}_t^T \mathbf{a}_t, \quad \frac{d}{dt}\mathbf{X}_t = \mathbf{V}_t$$
(4)

If we associate a matrix  $\mathbf{T}_t \in SE_2(3)$  to the extended pose  $(\mathbf{R}_t, \mathbf{V}_t, \mathbf{X}_t)$ , we noticed in [5] that (4) may be rewritten as

$$\frac{d}{dt}\mathbf{T}_t = \mathbf{W}_t \mathbf{T}_t + f(\mathbf{T}_t) + \mathbf{T}_t \mathbf{U}_t,$$
(5)

where the various matrices at play write

$$\mathbf{W}_{t} = \begin{pmatrix} 0_{3} & \mathbf{g} & 0\\ 0_{2,3} & 0_{2,1} & 0_{2,1} \end{pmatrix}, \quad \mathbf{U}_{t} = \begin{pmatrix} (\boldsymbol{\omega}_{t})_{\times} & \mathbf{a}_{t} & 0\\ 0_{2,3} & 0_{2,1} & 0_{2,1} \end{pmatrix}, 
f(\mathbf{T}_{t}) = \begin{pmatrix} 0_{3} & 0_{3,1} & \mathbf{V}_{t}\\ 0_{2,3} & 0_{2,1} & 0_{2,1} \end{pmatrix}.$$
(6)

It can be easily checked to verify the group-affine property:

**Definition 1 (Group-affine dynamics [5])** Let *G* be a Lie group. Dynamics  $\frac{d}{dt}\mathbf{T}_t = g(\mathbf{T}_t)$  on *G* is group-affine if it verifies for any couple  $\mathbf{T}, \tilde{\mathbf{T}} \in G$  the relation:

$$g(\mathbf{T}\tilde{\mathbf{T}}) = g(\mathbf{T})\tilde{\mathbf{T}} + \mathbf{T}g(\tilde{\mathbf{T}}) - \mathbf{T}g(Id)\tilde{\mathbf{T}}$$
(7)

This is the key property opening the door to invariant filtering, autonomous error variables, log-linearity and EKF stability leveraged in e.g. [17, 6]. The next section summarizes the links between the latter formulation of inertial navigation and the theory of preintegration of [25, 16]. Notably we have shown in [7] any equation of the form (5) on a matrix Lie group may in fact be preintegrated.

### 2.3 Preintegration of Group-Affine Dynamics

**Proposition 1 ([7] Corollary 9)** Assuming (5) are group-affine dynamics, or equivalently that  $f(\tilde{TT}) = f(T)\tilde{T} + Tf(\tilde{T})$ , which is the case with f as in (6) (both hand sides equal a matrix with  $R\tilde{V} + V$  in the rightmost block and null elsewhere), the solution  $T_t$  at arbitrary t of equation (5) can be written as a function of the initial value  $T_0$  as:

$$\mathbf{T}_t = \mathbf{\Gamma}_t \Phi_t(\mathbf{T}_0) \mathbf{\Upsilon}_t \tag{8}$$

where  $\Gamma_t$ ,  $\Upsilon_t$  are solution to differential equations involving only  $\mathbf{W}_t$ ,  $\mathbf{U}_t$ , and where  $\Phi_t$  only depends on t. Solving the corresponding equations (see [7]) in the particular case of equations (4) on  $SE_2(3)$  with values given by (6) yields

$$\Phi_t : \begin{pmatrix} \mathbf{R} & \mathbf{V} & \mathbf{X} \\ 0_{1,3} & 1 & 0 \\ 0_{1,3} & 0 & 1 \end{pmatrix} \mapsto \begin{pmatrix} \mathbf{R} & \mathbf{V} & \mathbf{X} + t\mathbf{V} \\ 0_{1,3} & 1 & 0 \\ 0_{1,3} & 0 & 1 \end{pmatrix},$$
(9)

$$\boldsymbol{\Gamma}_{t} = \begin{pmatrix} I_{3} & t\mathbf{g} & \frac{1}{2}\mathbf{g}t^{2} \\ 0_{1,3} & 1 & 0 \\ 0_{1,3} & 0 & 1 \end{pmatrix}, \ \boldsymbol{\Upsilon}_{t} = \begin{pmatrix} \mathbf{R}_{t}^{\upsilon} & \mathbf{V}_{t}^{\upsilon} & \mathbf{X}_{t}^{\upsilon} \\ 0_{1,3} & 1 & 0 \\ 0_{1,3} & 0 & 1 \end{pmatrix},$$
(10)

where the latter quantities are defined by

$$\mathbf{R}_{0}^{\upsilon} = I_{3}, \ \frac{d}{dt} \mathbf{R}_{t}^{\upsilon} = \mathbf{R}_{t}^{\upsilon}(\boldsymbol{\omega})_{\times}, \ \mathbf{V}_{0}^{\upsilon} = 0, \ \frac{d}{dt} \mathbf{V}_{t}^{\upsilon} = \mathbf{R}_{t}^{\upsilon} \mathbf{a}_{t},$$

$$\mathbf{V}_{0}^{\upsilon} = 0, \ \frac{d}{dt} \mathbf{X}_{t}^{\upsilon} = \mathbf{V}_{t}^{\upsilon}.$$
(11)

In [16], the quantities  $\mathbf{R}_t^{\upsilon}, \mathbf{V}_t^{\upsilon}, \mathbf{X}_t^{\upsilon}$  are referred to as the Delta preintegrated measurements and are based solely on the inertial measurements and do *not* depend on the initial state  $\mathbf{T}_0$ . This allows one to define constraints between extended poses at temporally distant key frames based on a *unique* (pre)integration of IMU outputs (11), no matter how many relinearizations are then used in the optimization scheme.

### **3** IMU preintegration with rotating earth

Many applications require accurate localization over long time scales based on accurate inertial sensors. To apply factor based optimization techniques to accurate inertial navigation systems requires to take into account the earth rotation and Coriolis effect. To this date, and to our best knowledge the theory of preintegration on manifolds cannot handle the corresponding equations exactly as the work of [16] is based on non rotating earth approximation based equations (4).

#### 3.1 IMU Equations with Rotating Earth are Group Affine

Accounting for earth rotation (4) becomes (see e.g. [15]):

1

$$\frac{d}{dt}\mathbf{R}_{t} = -\Omega_{\times}\mathbf{R}_{t} + \mathbf{R}_{t}(\boldsymbol{\omega})_{\times},$$

$$\frac{d}{dt}\mathbf{V}_{t} = \mathbf{g} + \mathbf{R}_{t}f_{t} - 2\Omega_{\times}\mathbf{V}_{t} - \Omega_{\times}^{2}\mathbf{X}_{t}, \quad \frac{d}{dt}\mathbf{X}_{t} = \mathbf{V}_{t}$$
(12)

where  $\Omega$  is the Earth rotation vector written in the local (geographic) reference frame. The term  $-2\Omega_{\times}^2 \mathbf{V}_t$  is called Coriolis force while the term  $-\Omega_{\times}^2 \mathbf{X}_t$  is called centrifugal force<sup>1</sup>. Eq. (12) does seemingly not lend itself to application of Prop. 1. However, if we introduce an auxiliary variable:

$$\mathbf{V}_t' = \mathbf{V}_t + \mathbf{\Omega}_{\times} \mathbf{X}_t \tag{13}$$

replacing velocity  $V_t$ , (12) unexpectedly simplifies to:

$$\frac{d}{dt}\mathbf{R}_t = -\mathbf{\Omega}_{\times}\mathbf{R}_t + \mathbf{R}_t(\boldsymbol{\omega})_{\times},$$
$$\frac{d}{dt}\mathbf{V}_t' = \mathbf{g} + \mathbf{R}_t f_t - \mathbf{\Omega}_{\times}\mathbf{V}_t', \quad \frac{d}{dt}\mathbf{X}_t = \mathbf{V}_t' - \mathbf{\Omega}_{\times}\mathbf{X}_t$$

This trick allows embedding the state into a matrix Lie group that fits into the framework of Eq. (5):

$$\frac{d}{dt}\mathbf{T}'_{t} = \mathbf{W}'_{t}\mathbf{T}'_{t} + f(\mathbf{T}'_{t}) + \mathbf{T}'_{t}\mathbf{U}_{t},$$
(14)

where matrix  $\mathbf{U}_t$  is unchanged and  $\mathbf{T}'_t, \mathbf{W}'_t$  write:

$$\begin{pmatrix} \mathbf{R}_t & \mathbf{V}_t' & \mathbf{X}_t \\ 0_{1,3} & 1 & 0 \\ 0_{1,3} & 0 & 1 \end{pmatrix}, \qquad \mathbf{W}_t = \begin{pmatrix} \Omega_{\times} & \mathbf{g} & 0 \\ 0_{2,3} & 0_{2,1} & 0_{2,1} \end{pmatrix}, \tag{15}$$

proving (12) are group affine, which is a novel result.

#### **3.2** Preintegration with Coriolis Effect

Using Proposition 1 we know the equations can be preintegrated. The explicit formulae, given in (16) below, may thus be derived along the lines of Section 2.

**Proposition 2 (Preintegration with Coriolis effect)** *The IMU equations* (12) *accounting for Coriolis and centrifugal force with initial state*  $\mathbf{R}_0$ ,  $\mathbf{V}_0$ ,  $\mathbf{X}_0$  *write exactly (no approximation is made):* 

$$\mathbf{R}_{t} = \mathbf{\Gamma}_{t}^{R} \mathbf{R}_{0} \mathbf{\Upsilon}_{t}^{R}$$
$$\mathbf{X}_{t} = \mathbf{\Gamma}_{t}^{x} + \mathbf{\Gamma}_{t}^{R} \mathbf{R}_{0} \mathbf{\Upsilon}_{t}^{x} + t \mathbf{\Gamma}_{t}^{R} \mathbf{V}_{0} + \mathbf{\Gamma}_{t}^{R} \mathbf{X}_{0}$$
$$\mathbf{V}_{t} = \mathbf{\Gamma}_{t}^{v} + \mathbf{\Gamma}_{t}^{R} \mathbf{R}_{0} \mathbf{\Upsilon}_{t}^{v} + \mathbf{\Gamma}_{t}^{R} \mathbf{V}_{0} - \mathbf{\Omega}_{\times} \mathbf{X}_{t}$$
(16)

<sup>&</sup>lt;sup>1</sup>To be perfectly accurate, this second term is the varying part of the centrifugal force, which actually writes  $-\Omega_{\times}^2(\mathbf{X}_t - p_0)$  with  $p_0$  a point of the Earth rotation axis. But expanding the parenthesis we obtain a constant term  $\Omega_{\times}^2 p_0$  which can be simply added to g. And this is already the case: the g we are familiar with (with approximate value 9.81m.s<sup>-2</sup>) is actually the sum of the Newton gravitation force and the centrifugal force due to Earth rotation. Hence the residual term  $-\Omega_{\times}^2 \mathbf{X}_t$ .

Where  $\Upsilon_t$  is the same as in (10) while  $\Gamma_t^R, \Gamma_t^v, \Gamma_t^x$  are defined through the following equations that do not involve the state:

$$\boldsymbol{\Gamma}_0^R = I_3, \quad \boldsymbol{\Gamma}_0^v = \boldsymbol{0}_{3,1}, \quad \boldsymbol{\Gamma}_0^x = \boldsymbol{0}_{3,1}; \quad \frac{d}{dt} \boldsymbol{\Gamma}_t^R = -\boldsymbol{\Omega}_{\times} \boldsymbol{\Gamma}_t^R,$$
$$\frac{d}{dt} \boldsymbol{\Gamma}_0^v = \boldsymbol{g} - \boldsymbol{\Omega}_{\times} \boldsymbol{\Gamma}_t^v, \quad \frac{d}{dt} \boldsymbol{\Gamma}_t^x = \boldsymbol{\Gamma}_t^v - \boldsymbol{\Omega}_{\times} \boldsymbol{\Gamma}_t^x.$$

**Proof** : We have to check the quantities defined by Eq. (16) verify Eq. (12).  $\frac{d}{dt}\mathbf{R}_t = -\Omega_{\times}\mathbf{R}_t + \mathbf{R}_t\omega_{\times}$  comes easily while we have, using matrix product differentiation rules and the definition of  $\Gamma_t$  and  $\Upsilon_t$  then rearranging terms:

$$\frac{d}{dt}\mathbf{X}_{t} = (\mathbf{\Gamma}_{t}^{v} + \mathbf{\Gamma}_{t}^{R}\mathbf{R}_{0}\mathbf{\Upsilon}_{t}^{v} + \mathbf{\Gamma}_{t}^{R}\mathbf{V}_{0}) - \mathbf{\Omega}_{\times}(\mathbf{\Gamma}_{t}^{x} + \mathbf{\Gamma}_{t}^{R}\mathbf{R}_{0}\mathbf{\Upsilon}_{t}^{x} + t\mathbf{\Gamma}_{t}^{R}\mathbf{V}_{0} + \mathbf{\Gamma}_{t}^{R}\mathbf{X}_{0})$$

which we recognize as  $\mathbf{V}_t$ . Now, differentiating  $\mathbf{V}_t$  the same way and using the relation  $\frac{d}{dt}\mathbf{X}_t = \mathbf{V}_t$  we obtain:

$$\frac{d}{dt}\mathbf{V}_t = \mathbf{g} + \mathbf{R}_t f_t - \Omega_{\times} (\Gamma_t^{\nu} + \Gamma_t^R \mathbf{R}_0 \boldsymbol{\Upsilon}_t^{\nu} + \Gamma_t^R \mathbf{V}_0 + \mathbf{V}_t).$$

But using the last equality of Eq. (16) we have  $\Gamma_t^v + \Gamma_t^R \mathbf{R}_0 \Upsilon_t^v + \Gamma_t^R \mathbf{V}_0 = \mathbf{V}_t + \Omega_{\times} \mathbf{X}_t$ and we end up with:

$$\frac{d}{dt}\mathbf{V}_t = \mathbf{g} + \mathbf{R}_t f_t - 2\Omega_{\times} \mathbf{V}_t - \Omega_{\times}^2 \mathbf{X}_t.$$

The latter novel mathematical results opens avenues for the application of factor based optimization methods such as GTSAM [13] or  $g^2o$  [23] to real time high performance localization and SLAM based on the use of precise IMUs, along the lines of [16].

**Remark 1** [21, 22] attacked factor graph based accurate navigation. The formulas for preintegration with Coriolis effect in the appendix of [22] are based on the early approach to preintegration [25], prior to the theory [16]. Preintegration formulas are not presented as exact, and are not indeed, as can be checked for instance propagating Eq. (35) of [22] for one time step, which yields:

$$v_{j+1}^{L_{j+1}} = R_{L_j}^{L_{j+1}} \left( v_j^{L_j} + R_{b_j}^{L_i} f_j \Delta t + \left[ g^{L_i} - 2 \left[ \omega_{iL_i}^{L_i} \right]_{\times} v_i^{L_i} \right] \Delta t \right).$$

We obtain a term  $-2\left[\omega_{iL_{i}}^{L_{i}}\right]_{\times}v_{i}^{L_{i}}$  in place of the expected  $-2\left[\omega_{iL_{i}}^{L_{i}}\right]_{\times}v_{j}^{L_{j}}$  (index i of v should be j): we see Coriolis term is actually approximated by its value at initial time  $t_{i}$ .

### **4** Associating uncertainty with extended poses

The goal of the present section is twofold. First, it shows how to account for noise in our approach to preintegration. Then, and more importantly, it provides a generalization of various methods and results of [2] devoted to SE(3) to the case of extended poses of  $SE_2(3)$ . This extension is independent from the theory of preintegration and is a contribution is itself. It is not trivial as even using the recently introduced  $SE_2(3)$  group IMU propagation is not amenable to Lie group compounding  $\mathbf{T}_{k+1} \exp(\boldsymbol{\xi}_{k+1}) = \mathbf{T}_k \exp(\boldsymbol{\xi}_k) \mathbf{\bar{T}} \exp(\boldsymbol{\xi})$  as considered in [2]. The unexpected log-linearity property of [5], that we rederive more simply below, plays a key role.

#### **4.1** Associating uncertainty with elements of $SE_2(3)$

Using the exponential map of SE(3) to describe statistical dispersion of poses has been largely advocated over past decades. In the robotics community, early attempts date back to [27], and the previously cited papers [11, 1, 12, 2, 29, 14, 3, 20, 26, 24] revolve around those ideas. Gaussians in exponential coordinates are also referred to as concentrated Gaussians, see e.g. [8]. We define a (concentrated) Gaussian on  $SE_2(3)$  as

$$\mathbf{T} = \bar{\mathbf{T}} \exp(\boldsymbol{\xi}),\tag{17}$$

where  $\bar{\mathbf{T}}$  is a noise free "mean" of the distribution and  $\boldsymbol{\xi} \sim \mathcal{N}(0, \boldsymbol{\Sigma})$  is a centered multivariate Gaussian in  $\mathbb{R}^9$ . Note indeed that, each component of  $\boldsymbol{\xi} = (\boldsymbol{\omega}^T, \mathbf{v}^T, \mathbf{x}^T)^T$  corresponds to a degree of freedom.

#### 4.2 Propagation of Errors through Noise Free IMU Model

We now come back to the widespread flat earth model (4) and consider discrete time, leveraging formula (8). In discrete time with time step  $\Delta t$ , denoting  $\Gamma_k := \Gamma_{\Delta t}$ ,  $\Phi := \Phi_{\Delta t}$  and  $\Upsilon_k := \Upsilon_{\Delta t}$ , we use (8) to get indeed

$$\mathbf{T}_{k+1} = \mathbf{\Gamma}_k \Phi(\mathbf{T}_k) \mathbf{\Upsilon}_k. \tag{18}$$

**Remark 2** Contrary to [16] our matrix group based preintegration formula (8) is an exact discretization of (4). However it involves (11) that need to by numerically solved at some point. As IMU measurements come in discrete time, albeit at a high rate, we may call  $\Delta t$  the discretization step and assume  $\mathbf{a}_t$ ,  $\omega_t$  to be constant over time intervals of small size  $\Delta t$ , along the lines of [16]. The solution to (8) is based on (11) whose solution then writes  $\mathbf{R}_{t+\Delta t}^{\upsilon} = \mathbf{R}_t^{\upsilon} \exp_m((\omega_t) \times \Delta t), \mathbf{V}_{t+\Delta t}^{\upsilon} =$   $\mathbf{V}_t^{\upsilon} + \mathbf{R}_t^{\upsilon} \mathbf{a}_t \Delta t$ , and  $\mathbf{X}_{t+\Delta t}^{\upsilon} = \mathbf{X}_t^{\upsilon} + \mathbf{V}_t^{\upsilon} \Delta t + \mathbf{R}_t^{\upsilon} \mathbf{a}_t \Delta t^2$  under the approximation of  $\mathbf{R}_t^{\upsilon}$  being also constant over  $\Delta t$  in the second equation.

We are now in a position to derive a preliminary yet remarkable result regarding propagation through noise free IMU equations of a concentrated Gaussian (17).

**Proposition 3 (Extended pose error propagation)** Let  $\mathbf{T}_k = \bar{\mathbf{T}}_k \exp(\boldsymbol{\xi}_k)$  where both  $\mathbf{T}_k$  and  $\bar{\mathbf{T}}_k$  evolve through noise free model (18). The propagation of discrepancy  $\boldsymbol{\xi}_k \in \mathbb{R}^9$  between  $\bar{\mathbf{T}}_k$  and  $\mathbf{T}_k$  writes  $\boldsymbol{\xi}_{k+1} = Ad_{\mathbf{\Upsilon}^{-1}}F\boldsymbol{\xi}_k$  with  $F(\boldsymbol{\omega}, \mathbf{v}, \mathbf{x})^T := (\boldsymbol{\omega}, \mathbf{v}, \mathbf{x} + \Delta t \mathbf{v})^T$ , i.e.,

$$\mathbf{T}_{k+1} := \mathbf{\Gamma}_k \Phi(\bar{\mathbf{T}}_k \exp(\boldsymbol{\xi}_k)) \mathbf{\Upsilon}_k = \bar{\mathbf{T}}_{k+1} \exp(Ad_{\mathbf{\Upsilon}_k^{-1}} F \boldsymbol{\xi}_k)$$
(19)

**Proof** : We have  $\mathbf{T}_{k+1} = \mathbf{\Gamma} \Phi(\bar{\mathbf{T}}_k \exp(\boldsymbol{\xi}_k)) \mathbf{\Upsilon}$ =  $\mathbf{\Gamma} \Phi(\bar{\mathbf{T}}_k) \Phi(\exp(\boldsymbol{\xi}_k)) \mathbf{\Upsilon}$  where we used the fact that  $\Phi(\mathbf{T}_1 \mathbf{T}_2) = \Phi(\mathbf{T}_1) \Phi(\mathbf{T}_2)$  as shown by simple computations based on (9). Thus  $\mathbf{T}_{k+1} = \mathbf{\Gamma} \Phi(\bar{\mathbf{T}}_k) \mathbf{\Upsilon} \mathbf{\Upsilon}^{-1} \Phi(\exp(\boldsymbol{\xi}_k)) \mathbf{\Upsilon} = \bar{\mathbf{T}}_{k+1} A d_{\mathbf{\Upsilon}^{-1}} (\Phi(\exp(\boldsymbol{\xi}_k)))$ . Using the expression (1) for the exponential map and (9) we see that

$$\Phi(\exp(\boldsymbol{\xi})) = \exp(F\boldsymbol{\xi}) \tag{20}$$

where  $F(\boldsymbol{\omega}, \mathbf{v}, \mathbf{x})^T = (\boldsymbol{\omega}, \mathbf{v}, \mathbf{x} + \Delta t \mathbf{v})^T$ . Using that matrix exponential commutes with conjugation we get  $Ad_{\Upsilon^{-1}}(\exp(F\boldsymbol{\xi})) = \exp(Ad_{\Upsilon^{-1}}F\boldsymbol{\xi})$ , proving the result. We have just proved in discrete time using elementary means the log-linear property of [5] dealing with continuous time. It proves the interest of error representation (17) using exponential coordinates in  $SE_2(3)$ , as (19) shows the errors  $\boldsymbol{\xi}_k$ expressed using those coordinates in  $\mathbb{R}^9$  propagate *linearly* in exponential coordinates (as (2) proves that  $Ad_{\Upsilon^{-1}}F \in \mathbb{R}^{9\times 9}$ ) through IMU equations (8) and hence (4).

**Remark 3** In propagation by compounding, i.e.  $\exp(\boldsymbol{\xi}_{k+1})\mathbf{T}_{k+1} = \exp(\boldsymbol{\xi})\bar{\mathbf{T}}\exp(\boldsymbol{\xi}_k)\mathbf{T}_k$ instead of more sophisticated dynamics (18), it was already proved at Eq. (26) of [2] noise free propagation, i.e.  $\boldsymbol{\xi} = 0$  in the above, preserves statistical distributions (17) and it also explains why actual dispersion of wheel robots is banana shaped, see [24, 2]. Herein the result is recovered (letting  $\Gamma = \bar{\mathbf{T}}, \Upsilon = Id$  and  $\Phi(\mathbf{T}) = \mathbf{T}$ ) and we provide an extension to the actual IMU propagation (4). This is not trivial since it first requires to transform (4) into (18), a recent advanced result, and then  $\Phi$  cannot be broken into simple multiplications. However, we leveraged the fact it is a group automorphism.

#### 4.3 Propagation with Noisy IMU: an Exact Formula

The theory allows deriving a novel result describing error accumulation over time. When IMU noise is accounted for in (18) we get (a justification will be given in Section 4.4):

$$\mathbf{T}_{k+1} = \mathbf{\Gamma}_k \Phi(\mathbf{T}_k) \mathbf{\Upsilon}_k \exp(w_k), \tag{21}$$

with  $w'_i s$  independent Gaussian noises. The group-affine property of the  $SE_2(3)$  embedding allows deriving a novel result describing error accumulation over time.

**Proposition 4 (Extended pose error accumulation)** Referring to (17) let us write  $\mathbf{T}_k$  as  $\mathbf{T}_k = \bar{\mathbf{T}}_k \exp(\boldsymbol{\xi}_k)$  where  $\bar{\mathbf{T}}_k$  is propagated through noise free equations (18) *i.e.*,  $\bar{\mathbf{T}}_{k+1} = \Gamma_k \Phi(\bar{\mathbf{T}}_k) \Upsilon_k$ . Let  $F_i := Ad_{\Upsilon_k^{-1}} F \in \mathbb{R}^{9 \times 9}$  and  $F_i^k := \Pi_{j=i}^{k-1} F_j$ . We have the recursive formula

$$\exp(\boldsymbol{\xi}_{k+1}) = \exp(F_k \boldsymbol{\xi}_k) \exp(w_k) \tag{22}$$

leading to the following exact formula:

$$\exp(\boldsymbol{\xi}_k) = \exp(F_0^{k-1}\boldsymbol{\xi}_0) \cdot \prod_{i=0}^{k-1} \exp(F_i^{k-1}w_i).$$
(23)

**Proof:** Juste before (20) we proved  $\exp(\boldsymbol{\xi}_{k+1}) = Ad_{\boldsymbol{\Upsilon}_k^{-1}}(\Phi(\exp(\boldsymbol{\xi}_k)))$  for noise free model (18). With noisy model (21) we have along the same lines

$$\exp(\boldsymbol{\xi}_{k+1}) = Ad_{\boldsymbol{\Upsilon}^{-1}}(\Phi(\exp(\boldsymbol{\xi}_k)))\exp(w_k).$$
(24)

Moreover at (20) and following lines we proved

$$Ad_{\mathbf{\Upsilon}_{k}^{-1}} \circ \Phi(\exp(\boldsymbol{\xi})) = \exp(Ad_{\mathbf{\Upsilon}_{k}^{-1}}F\boldsymbol{\xi})$$
(25)

readily proving (22). Moreover we proved  $\Phi(\mathbf{T}_1\mathbf{T}_2) = \Phi(\mathbf{T}_1) \cdot \Phi(\mathbf{T}_2)$ , i.e.  $\Phi$  is an automorphism, and so is the adjoint, and the composition of automorphisms is an automorphism, so  $Ad_{\Upsilon-1} \circ \Phi$  satisfies the same property. Using all the latter results and denoting  $Ad_{\Upsilon_k^{-1}} \circ \Phi$  by  $\Psi_k$  we have

$$\exp(\boldsymbol{\xi}_2) = Ad_{\boldsymbol{\Upsilon}_1^{-1}} \circ \Phi\left(Ad_{\boldsymbol{\Upsilon}_0^{-1}} \circ \Phi(\exp \boldsymbol{\xi}_0) \exp(w_0)\right) \exp(w_1)$$
  
=  $\Psi_1\left(\Psi_0(\exp \boldsymbol{\xi}_0)\right) \exp(w_0) \exp(w_1)$   
=  $\Psi_1(\Psi_0(\exp \boldsymbol{\xi}_0))\Psi_1(\exp(w_0)) \exp(w_1)$   
=  $\exp(F_1F_0\boldsymbol{\xi}_0))\exp(F_0w_0))\exp(w_1)$ 

and (23) is proved by recursion along the same lines.

This result is remarkable: having a simple closed-formula for the error propagation is not usual in nonlinear state estimation. A first application is that the result of [2] for pose compounding based on the use of the full BCH formula also holds true for inertial navigation: if the initial error  $\xi_0$  and the noises  $w_i$  are centered on zero then the propagated error is centered up to the third order w.r.t. the standard deviation of  $\xi_0$  and the  $w_i$ 's, which is another argument advocating the relevance of our uncertainty representation.

#### 4.4 Justification for Noise Model and Approximation

Noisy IMU model (21) may be justified as follows. In practice IMU measure the quantities  $\tilde{\mathbf{a}}_k := \mathbf{a}_k - \mathbf{b}_k^a - \eta_k^a$  and  $\tilde{\boldsymbol{\omega}}_k := \boldsymbol{\omega}_k - \mathbf{b}_k^g - \eta_k^g$  where  $\mathbf{b}_k = (\mathbf{b}_k^g, \mathbf{b}_k^a) \in \mathbb{R}^6$  denotes the gyrometers and accelerometers biases, and  $\boldsymbol{\eta}$  represent sensor noise. For now, let's assume  $\mathbf{b} = 0$ , as biases will be the focus of Section 5. From (11) we have to the first order in  $\Delta t$ :

$$\mathbf{\Upsilon} = \begin{pmatrix} \exp(\tilde{\boldsymbol{\omega}}\Delta t)_{\times} & \tilde{\mathbf{a}}\Delta t & \mathbf{0}_{3,1} \\ \mathbf{0}_{1,3} & 1 & \mathbf{0} \\ \mathbf{0}_{1,3} & \mathbf{0} & 1 \end{pmatrix}.$$
 (26)

A simple matrix multiplication proves that this implies the following first order relation between factor  $\Upsilon$  associated to noisy inertial increments and  $\overline{\Upsilon}$  associated to noise free ones

$$\Upsilon \approx \bar{\Upsilon} \exp(\eta^{g} \Delta t, \eta^{a} \Delta t, 0) := \bar{\Upsilon} \exp(\eta_{k}), \qquad (27)$$

and we let  $\eta_k := (\eta_k^g \Delta t, \eta_k^a \Delta t, 0) \in \mathbb{R}^9$ . Recalling (18), we then have in the presence of IMU noise the motion model:

$$\mathbf{T}_{k+1} = \boldsymbol{\Gamma} \boldsymbol{\Phi}(\mathbf{T}_k) \, \bar{\boldsymbol{\Upsilon}} \exp(\boldsymbol{\eta}_k), \tag{28}$$

and we now seek to describe how the distribution (17), i.e., associated parameters  $\overline{\mathbf{T}}, \Sigma$ , propagate through it.

Although it be unusual to be able to come up with exact formulas such as (23), the formula is still nonlinear and does not readily provide the evolution of  $\xi_k$ 's covariance.

**Proposition 5 (IMU noise propagation)** Consider a sequence of uncertain extended poses, modeled as  $\mathbf{T}_k = \bar{\mathbf{T}}_k \exp(\boldsymbol{\xi}_k)$  with  $\boldsymbol{\xi}_k \sim \mathcal{N}(0, \boldsymbol{\Sigma}_k)$ . Using the BCH formula to the first order in (22) readily provides an approximation of uncertainty propagation through noisy IMU model (28) as

$$\bar{\mathbf{T}}_{k+1} = \boldsymbol{\Gamma}_k \boldsymbol{\Phi}(\bar{\mathbf{T}}_k) \boldsymbol{\Upsilon}_k, \quad \boldsymbol{\Sigma}_{k+1} = F_k \boldsymbol{\Sigma}_k F_k^T + \boldsymbol{\Sigma}_{\boldsymbol{\eta}}.$$
(29)

Up to the first order, the obtained Riccati equation agrees with the results of [16], see appendix therein. However, at higher order formulas are different owing to the exponential and the choice of uncertainty representation.

In the presence of IMU noise, the true distribution is not exactly described by our uncertainty representation. However, the fact propagation be exact in deterministic propagation (Proposition 3) is a good indication our uncertainty representation combined with Riccati equation (29) provides an accurate description of dispersion. This is also supported by the simple numerical experiment of Figure 1 where we see true and computed dispersions match.

## 5 Impact of biases in exponential coordinates for preintegration

In this section, we compute first order biais correction using our representation of errors based on exponential coordinates on  $SE_2(3)$ . First, our matrix formalism allows for more elementary computations than the first order expansions that can be found in the Appendix of [16]. Second our theory yields slightly more accurate Jacobians for first-order bias correction in the theory of preintegration.

#### 5.1 Theory

Consider full IMU measurements  $\tilde{\mathbf{a}}_k := \mathbf{a}_k - \mathbf{b}_k^a - \eta_k^a$  and  $\tilde{\boldsymbol{\omega}}_k := \boldsymbol{\omega}_k - \mathbf{b}_k^g - \eta_k^g$ , and let us ignore the noise and focus only on the biases. In the context of smoothing, given a bias update  $\mathbf{\bar{b}} \leftarrow \mathbf{\bar{b}} + \delta \mathbf{b}$ , one needs to compute how the preintegrated quantities change. Assume we have computed the extended pose  $\mathbf{T}_k(\mathbf{\bar{b}})$  at time *k* corresponding to bias  $\mathbf{\bar{b}}$  and let  $\mathbf{T}_k(\mathbf{\hat{b}})$  denote the extended pose associated to new bias estimation  $\mathbf{\hat{b}} := \mathbf{\bar{b}} + \delta \mathbf{b}$  with  $\delta \mathbf{b} = (\delta \mathbf{b}^g, \delta \mathbf{b}^a) \in \mathbb{R}^6$ . Building upon our exponential representation of errors on  $SE_2(3)$  (17) in a stochastic context, we define the discrepancy between those two extended poses as  $\mathbf{d}_k \in \mathbb{R}^9$ , i.e.,

$$\mathbf{T}_k(\hat{\mathbf{b}}) = \mathbf{T}_k(\bar{\mathbf{b}}) \exp(\mathbf{d}_k), \tag{30}$$

and we seek how this correction evolves with time. Denote  $\Upsilon(\mathbf{b})$  the quantity obtained by replacing  $(\tilde{\boldsymbol{\omega}}, \tilde{\mathbf{a}})$  with  $(\tilde{\boldsymbol{\omega}} + \mathbf{b}^g, \tilde{\mathbf{a}} + \mathbf{b}^a)$  in (26). Neglecting  $O(\Delta t^2)$  terms yields

$$\Upsilon(\hat{\mathbf{b}}) \approx \Upsilon(\bar{\mathbf{b}}) \exp(\delta b^g \Delta t, \delta b^a \Delta t, 0).$$
(31)

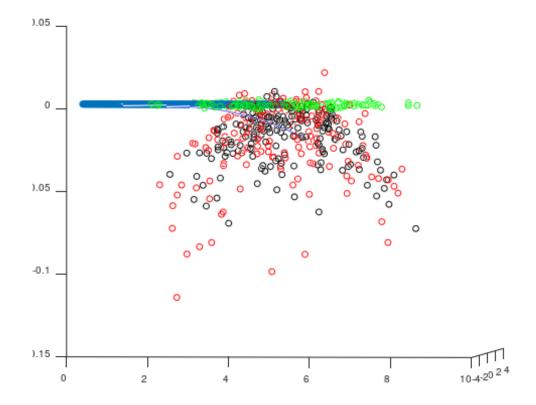


Figure 1: Numerical experiment to support uncertainty propagation model (29) coupled with uncertainty representation (17). The initial extended pose is null and known, and the IMU moves nominally to the right at constant translational speed (blue line). Noisy IMU measurements generate a dispersion of the belief at the endpoint. We generate point clouds at the trajectory endpoint based on Monte-Carlo simulations. Black dots represent true dispersion under noisy equations (4). Red dots are generated through our exponential uncertainty model (17) for extended pose propagation with parameters computed via (29). Finally green dots are generated using the endpoint distribution computed by a standard (multiplicative) EKF: we see linearization implies the assumed dispersion lies within a horizontal plane. However, the true distribution (black) is "banana" shaped in 3D, as already observed mainly in the case of poses in 2D for wheeled robots [24, 11, 1, 12, 2], and (29) captures this effect and agrees with ground truth.

Thus using (18), (30) and (31) we get

$$\mathbf{T}_{k+1}(\hat{\mathbf{b}}) = \mathbf{\Gamma}_k \Phi(\mathbf{T}_k(\hat{\mathbf{b}})) \boldsymbol{\Upsilon}_k(\hat{\mathbf{b}})$$
(32)

$$= \mathbf{\Gamma}_k \Phi(\mathbf{T}_k(\bar{\mathbf{b}}) \exp(\mathbf{d}_k)) \mathbf{\Upsilon}_k(\bar{\mathbf{b}}) \exp(\bar{\boldsymbol{\delta}}\bar{\boldsymbol{b}}).$$
(33)

where  $\bar{\delta b} := (\delta b^g \Delta t, \delta b^a \Delta t, 0) \in \mathbb{R}^9$ . Using (19) we get

$$\mathbf{T}_{k+1}(\hat{\mathbf{b}}) = \mathbf{T}_{k+1}(\bar{\mathbf{b}}) \exp(Ad_{\mathbf{\Upsilon}_k(\bar{\mathbf{b}})^{-1}}F\mathbf{d}_k) \exp(\bar{\delta b})$$
(34)

$$\approx \mathbf{T}_{k+1}(\bar{\mathbf{b}}) \exp(Ad_{\mathbf{\Upsilon}_{k}(\bar{\mathbf{b}})^{-1}}F\mathbf{d}_{k} + \bar{\delta}\bar{\mathbf{b}}), \tag{35}$$

where we used the BCH formula. We have thus proved the discrepancy  $\mathbf{d}_k$  in the sense of (30) between extended poses respectively associated to biases  $\mathbf{\bar{b}}$  and  $\mathbf{\hat{b}} = \mathbf{\bar{b}} + \delta \mathbf{b}$  satisfies over time the incremental equation:

$$\mathbf{d}_{k} = J_{k} \bar{\boldsymbol{\delta}} \mathbf{b}, \text{ where } J_{k+1} = A d_{\boldsymbol{\Upsilon}_{k}(\bar{\mathbf{b}})^{-1}} F J_{k} + I_{9,6}$$
(36)

Where  $I_{9,6}$  is a 6 × 6 identity matrix concatenated with a 3 × 6 matrix of zeros. We see the only approximation<sup>2</sup> comes in at line (35).

**Remark 4** Neglecting terms in  $\Delta t^2$  in (31) alleviates computations but is not fully accurate. For correct expansion w.r.t.  $\delta \bar{b}$  the diagonal identity blocks  $1: 3 \times 1: 3$  and  $4: 6 \times 4: 6$  of matrix  $I_{9,6}$  should be replaced with  $\Delta tD$  and  $\Delta texp_m((\omega_t) \times \Delta t)$  respectively, where D is defined by the expansion  $exp_m((\omega + u)_{\times}) = exp_m(\omega)[I_3 + (Du)_{\times} + \circ(u)].$ 

The following result is already true for classical Taylor expansion of [16], although it seems to have gone unnoticed.

**Proposition 6** In absence of gyro bias both formulas (31) and (35) are exact, meaning we have exact pre-integration where accelerometer bias is fully modeled.

#### 5.2 Numerical comparison

We showed the exponential mapping on  $SE_2(3)$  more closely reflects uncertainty when using noisy IMUs. In turn, one may wonder if using the exponential to model bias correction (30) improves accuracy. The answer turns out to be positive, although the improvement is rather slight.

We set a simple simulation where a UAV follows a 3D trajectory (see Fig. 2) while recording IMU measurements, and storing preintegrated factors, each covering a duration *T*. The original sampling frequency is 100Hz, so T = 0.01 means

<sup>&</sup>lt;sup>2</sup>besides the Euler approximation (31) justified by small  $\Delta t$ .

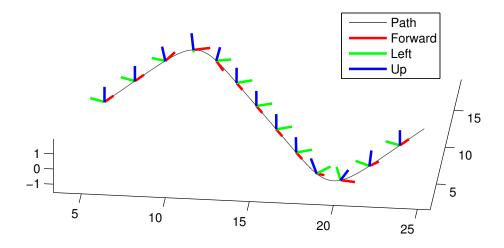


Figure 2: Simulated trajectory

| Table 1: Higher-o | order errors | for a low-cost | : IMU (1° | (s - 100mg) |
|-------------------|--------------|----------------|-----------|-------------|
|                   |              |                |           |             |

| IMU       | Velocity RMS (m/s) |             |             | Position RMS (m) |             |             |
|-----------|--------------------|-------------|-------------|------------------|-------------|-------------|
| Т         | 1s                 | 10 <i>s</i> | 60 <i>s</i> | 1 <i>s</i>       | 10 <i>s</i> | 60 <i>s</i> |
| Classical | $6,9.10^{-3}$      | 1,25        | 151,5       | 0,0016           | 3,66        | 2405,8      |
| Proposed  | $9,375.10^{-4}$    | 0,37        | 70,5        | 0,0015           | 2,57        | 2126,5      |

all measurements are stored. Then we sample values of the gyro and accelerometer bias and compute the difference between preintegrated factors obtained reintegrating the IMU increments and pre-integrated factors obtained through the two first-order expansion, as in standard preintegration theory [16] and exponential as in (30), (36). Results for the velocity and position components of the pre-integrated factors are displayed on Table 1 for a bias corresponding to a low-cost IMU. We see the exponential mapping of our group theoretic approach tends to improve velocity accuracy of the first-order expansion. As the errors between the preintegrated factors and their first-order approximation are very small for a standard pre-integration time of T = 1s, so we conclude that regarding bias correction exponential mapping may prove useful in specific situations such as long term preintegration.

## 6 Conclusion

We showed the properties of  $SE_2(3)$  allow transposing the rather recent results about estimation of poses using wheel speeds to the context of IMUs. Moreover, the framework provides an elegant mathematical approach that brings further maturity to the theory of preintegration on manifolds. It unifies flat and rotating earth IMU equations within a single framework, hence providing extensions of the theory of preintegration to the context of high grade IMUs and opening up for novel implementations of factor graph based methods to high precision (visual) inertial navigation systems.

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