

# Cemef

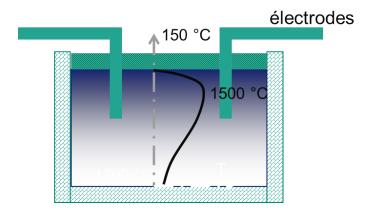
July, 13th 2018, Saint-Malo ■ ■

■ Thermoconvective instabilities of a non uniform Joule-heated liquid enclosed in a rectangular cavity

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# **Motivations of the present work**

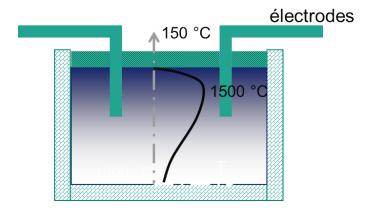




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### **Motivations of the present work**





Joule dissipation provides the heating; The maximum of T is observed in the bulk; Thermically instable.



#### 1. Problem statement

- 2. Steady-state solutions for  $L_e/H = 1$
- 3. Onset of convection when  $L_e/H < 1$
- 4. Instabilities in a cavity with  $L_e/H = 2/3$
- 5. Conclusion

### 1. Problem statement I





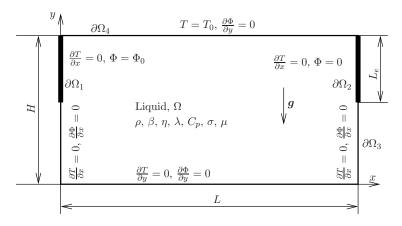


Figure 1: Cavity  $\Omega$  filled with an electric conductor liquid according to Sugilal, G., et al. (2005). [*Int. J. Therm. Sci.*, **44**:915-925].

#### 1. Problem statement II



#### Assumptions

- Boussinesq approximation is used to take into account the buoyancy force.
- Effects of induced magnetic field B are neglected.
- The Lorentz forces are neglected.

#### Normalization of the problem

- x normalized by H;
- $t \text{ by } H^2/\kappa \text{ with } \kappa = \lambda/(\rho C_p);$
- **u** by  $\sqrt{\beta \Delta TgH}$ ;

$$\theta = \frac{T - T_0}{\Delta T}$$
, with  $\Delta T = \frac{\sigma \Phi_0^2 H^2}{2\lambda L^2}$ . (1)

#### 1. Problem statement III



#### Balance equations



$$\nabla \cdot \mathbf{u} = 0, \qquad (2)$$

$$\frac{1}{\Pr} \frac{\partial \boldsymbol{u}}{\partial t} + \sqrt{\frac{\operatorname{Ra}}{\Pr}} \boldsymbol{u} \cdot \nabla \boldsymbol{u} = -\nabla \rho + \nabla^{2} \boldsymbol{u} + \sqrt{\frac{\operatorname{Ra}}{\Pr}} \theta \boldsymbol{e}_{y}, \qquad (3)$$

$$\frac{\partial \theta}{\partial t} + \sqrt{\operatorname{Pr} \operatorname{Ra}} \nabla \theta \cdot \boldsymbol{u} = \nabla^{2} \theta + 2L^{2} (\nabla \Phi)^{2}, \qquad (4)$$

$$\nabla^{2} \Phi = 0. \qquad (5)$$

$$\frac{\partial \theta}{\partial t} + \sqrt{\operatorname{Pr} \operatorname{Ra}} \nabla \theta \cdot \boldsymbol{u} = \nabla^2 \theta + 2L^2 (\nabla \Phi)^2, \qquad (4)$$

$$\nabla^2 \Phi = 0. \tag{5}$$

#### **Dimensionless numbers**

$$Ra = \frac{\beta g \Delta T H^3}{\nu \kappa}, \tag{6}$$

$$Pr = \frac{\nu}{r}.$$
 (7)

# 2. Steady-state solutions for $L_e/H = 1$



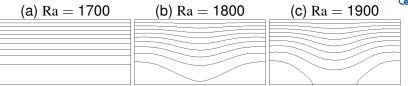


Figure 2: Isolines of  $\theta$  for (a) Ra = 1700, (b) Ra = 1800 and (c) Ra = 1900.

- $ightharpoonup Ra_{cr} = 1702.$
- By linear stability, Kulacki and Goldstein<sup>1</sup> found Ra<sub>cr</sub> = 1386.
- ▶ Numerically, Sugilal et al. (2005) found Ra<sub>cr</sub> = 1650.

<sup>&</sup>lt;sup>1</sup>Kulacki, F. A. & Goldstein, R. J. (1975). Appl. Sci. Res., **31**:81-109.

# 2. Steady-state solutions for $L_e/H=1$



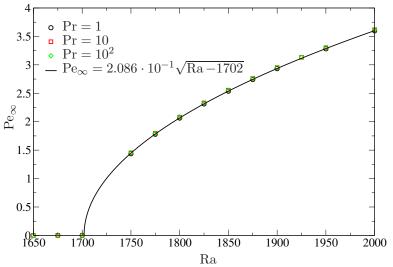
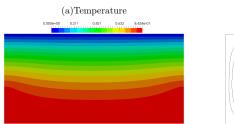


Figure 3:  $Pe_{\infty} = U_{max}H/\kappa$  vs. Ra for L/H=2,  $L_e/H=1$  and Pr=1, 10 and 100.





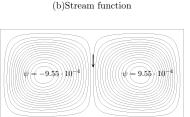
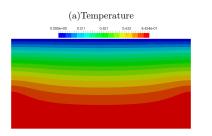


Figure 4: (a)  $\theta \in [0, 0.84]$  and (b) stream function  $\psi$  for Pr = 1, Ra =  $10^2$  and  $L_e = 2/3$ .





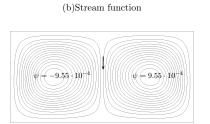


Figure 4: (a)  $\theta \in [0, 0.84]$  and (b) stream function  $\psi$  for Pr = 1, Ra =  $10^2$  and  $L_e = 2/3$ .

▶ The threshold disappears when  $L_e/H < 1$ .

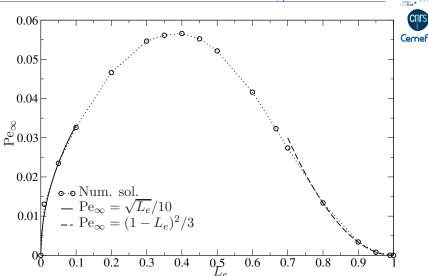


Figure 5:  $Pe_{\infty}$  vs.  $L_e$  for Pr = 1 and  $Ra = 10^2$ .



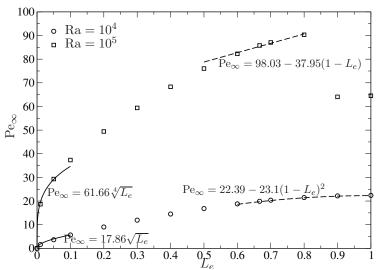


Figure 6:  $Pe_{\infty}$  vs.  $L_e$  in the situation where  $Ra=10^4$  or  $10^5$  and for Pr=1.



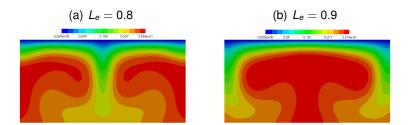


Figure 7: Temperature field obtained for Ra =  $10^5$ , Pr = 1 and for (a)  $L_e = 0.8$ ,  $\theta \in [0; 0.39]$  and (b)  $L_e = 0.9$ ,  $\theta \in [0; 0.36]$ .



### Numerical solution for $Ra = 4 \cdot 10^4$ and $Pr = 10^2$

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- 1. Steady symmetric structure;
- 2. Steady asymmetric structure;
- 3. Unsteady asymmetric structure.



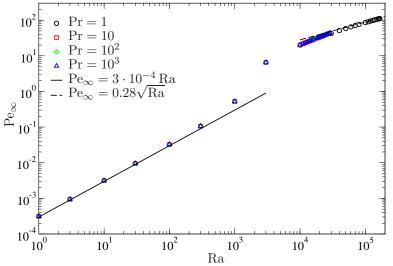


Figure 8:  $Pe_{\infty}$  vs. Ra and Pr = 1, 10,  $10^2$  and  $10^3$ .



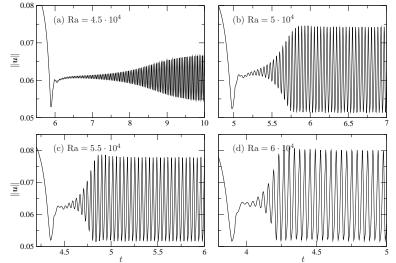


Figure 9:  $\|u\|$  vs. t for Pr = 10 and (a) Ra =  $4.5 \cdot 10^4$ , (b) Ra =  $5 \cdot 10^4$ , (c) Ra =  $5.5 \cdot 10^4$  and (d) Ra =  $6 \cdot 10^4$ .



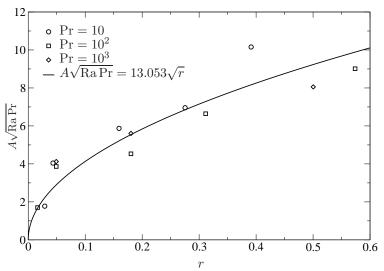


Figure 10: Fundamental amplitude of Fourier spectra  $A\sqrt{Ra\,Pr}$  vs.  $r=(Ra-Ra_{cr_2})/Ra_{cr_2}$  for  $Pr=10,\,10^2$  and  $10^3$ .



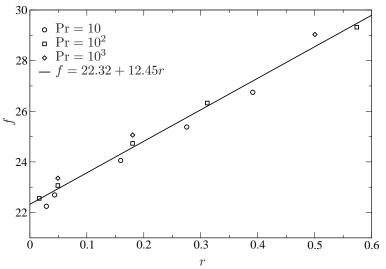


Figure 11: Fundamental frequency of Fourier spectra f vs.  $r = (Ra - Ra_{cr_2})/Ra_{cr_2}$  for  $Pr = 10, 10^2$  and  $10^3$ .



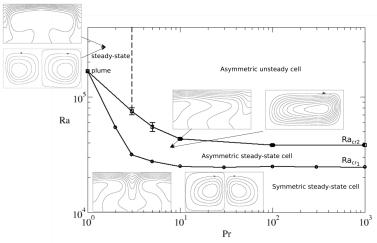


Figure 12: Stability diagram (Pr,  $Ra_{cr_{1,2}}$ ) describing the three main structures obtained numerically when  $L_e = 2/3$ .

### 5. Conclusion



- ▶ If  $L_e/H = 1$ , the critical Rayleigh number is:  $Ra_{cr} = 1702$ .
- ▶ If  $L_e/H < 1$ , convection without threshold.
- Three instabilities are established:
  - The first one is similar to the transcritical bifurcation.
  - The second is subcritical bifurcation.
  - The third is similar to the Hopf bifurcation.
- From the results of oscillation frequencies, we can find:
  - with physical properties of glass wool,  $t_{\rm osc} \approx 1$  h.
- Heat transfer has been also studied<sup>2</sup>.
- To be verified in industrial plants.
- Extend this work to 3D configuration.

<sup>&</sup>lt;sup>2</sup>Pigeonneau, F., Cornet, A. & Lopépé, F. (2018). *J. Fluid Mech.*, **843**:601–636.