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An Advanced 3D Mathematical Model for a 6-high Tandem Cold Rolling Process

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Abstract

The present paper focuses on the validation of on-going efforts made to develop more advanced 3D mathematical model for cold rolling strip process [8]. Following [2], the model uses the multi-slab strategy to deal with the differential reduction in the transverse direction due to roll deformation, and analytical solutions of roll bending and flattening discretized by the Influence Function Method (IFM). Furthermore, the model has been extended to incorporate elastic deformation of strip and to be fit for 6-high rolling mills with shiftable work roll (WR) or Intermediate Rolls (IR) as well as 4-high mills. Validation is performed by using FEM solutions (Abaqus® implicit) as references: a 2D quasi-static model to check the slab method under rigid work roll condition; a 3D FEM to discuss the assumption of small lateral flow of strip; a comparison of FEM and IFM with regard to 6-high roller stack deformation with intermediate roll shifting. All these steps are essential to gain more insight into the mechanism of cold rolling strip and to guide future development work of the mathematical model.

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Keywords: Cold rolling strip; Slab method; Influence Function Method; Finite Element Method

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1. Introduction

Modern steel strip cold rolling involves tandem mills consisting of typically five successive six-high (6 rolls) stands with complex actuations : at each stand, work roll (WR) and intermediate roll (IR) shifting, roll bending forces (FRB) allow fast adaptation whereas roll grinding crown brings a constant, first order correction to roll bending and flattening. These are necessary, powerful tools for an optimal strip profile and flatness, but modelling is needed to design their multivariable control system.

For this particularly important metal forming process, a number of models have been developed for a long time, see e.g. [1-3] and a review in [4]. However on modern mills, WR and IR roll shifting make it a fully 3D problem in which planar symmetries are replaced by skew symmetry, requiring extension into more general models. Moreover, rolling harder steel grades results in higher stresses, calling for more robust deformation models. Finally, due to the large number of parameters to be included in the design procedure, these mathematical models must bring about a high quality/cost ratio to allow intensive parametric studies.

Many methods are currently used to model strip deformation: Slab Method (SM) in 2D, Upper Bound Method (UBM) or Finite Element Method (FEM) for both 2D and 3D; an asymptotic approach has also been applied to the calculation of 2D strip deformation [5], offering interesting mathematical insight but with limited practical capacities. To model roll bending, researchers use either the beam theory or the FEM, whereas flattening is calculated by e.g. Boussinesq's analytical equations or the FEM. Most recently, a boundary element method using the Mindlin's solution has been proposed to solve the elastic flattening deformation of the whole roll stack [6]; however to cope with complex boundary conditions, these authors had to introduce FEM-based approximate corrections, just as in the semi-analytical model of Hacquin [3] which therefore remains as precise and faster.

To deal with the whole (strip + rolls + actuators) problem, any combination of these bricks can be, and has been, proposed, the coupling technique being an essential ingredient [4]. This has been done using e.g. the FEM [7] for the whole systems but the cost is very high. The present paper is inspired from Pawelski's work [2], whereby a semi-analytical model of the roll deformation is discretized by the Influence Function Method (IFM) whereas a series of longitudinal 2D slabs modelled with the SM deal with the differential reduction across the width induced by roll bending and flattening. Such approaches to predict rolled strip crown have been experimentally validated in the past under various rolling conditions for mild steel relatively thick strips. In a previous paper [8], the present authors have improved the accuracy of the model of [2] by relaxing Hitchcock's assumption of circular work roll surface and adding discretization technique of Influence Function Method in rolling direction, in an effort to address harder and thinner strips in the future. The present paper is devoted to the validation of two bricks of the model. First, the elastic-plastic SM is compared with 2D plane strain FEM. Secondly, 3D FEM is used to check (1) the assumption of viewing strip as a series of slabs at different transverse positions and (2) the roll stack elastic deformation model based on the Influence Function Method (IFM).

Nomenclature

| | |
|---------------|--|
| x, y, z | Cartesian coordinates in the rolling, transverse and thickness direction, respectively |
| ε | strain, upper script p for plastic strain |

2. Brief models description

2.1. Strip deformation

The present Slab Model is based on the variant proposed by Le and Sutcliffe [9] (where full details can be found) of the SM initiated by von Karman in 1925. The main assumptions are plane strain and stress uniformity in the normal direction (z), resulting in a 1D ordinary differential equation (ODE) in the normal and tangential stress. The friction stress is expressed by a Coulomb law; the stick / slip kinematical transition is smoothed by a regularization technique [10] using the tangential relative velocity. An elastic-plastic model is used, based on Prandtl-Reuss additive decomposition of the strain rate and including work-hardening. Taking the back tension as initial condition,

the ODE is integrated; due to the change of the sign of friction at the unknown location of the neutral point, an iterative procedure is needed to ensure that the exit stress matches the front tension: a bisection method is used for the initial two iterations, a secant method further on.

It must be noted that special care must be taken when rolling hard and thin material, because of the large elastic deformation of WR which may result in a central elastic zone (or “contained plastic”, or “no-slip”) inserted between the entry and exit plastic zones (with further elastic zones at entry and exit of course). The integration with changing sets of equations proves difficult in the central area due to spurious sign change of the local roll profile slope under extreme contact pressures. Therefore, [9] inverts the scheme in the central area and deduce normal and tangential stresses not from equilibrium equation integration, but from the no-slip condition, both strip and roll being elastic. This option is however not used in the present paper which is thus limited to rolling of thicker strips.

2.2. IFM model of roll stack deformation

For 4/6 high roll stacks, the authors follow the 3D semi-analytical elastic roll deformation model fully described by Hacquin et al. [3,4]. It combines roll bending based on Timoshenko’s beam theory, roll flattening based on Boussinesq’s equations for a semi-infinite solid arbitrarily loaded on its surface, Hertz contact theory for the roll - roll contact. End effect for the complex geometry and boundary conditions of the roll barrel edge have been corrected by analytical expressions derived from extensive FEM comparisons. All equations are discretized by a 3D influence function method. Due to the unknown roll – roll contact areas, the resulting equations are non-linear and are solve by Newton-Raphson scheme.

3. Result and discussion

3.1. Plane strain study: validation of Slab Method against FEM

Table 1. Parameters used for the rolling pass

| Variables | Value |
|------------------------------|-----------------------------------|
| Inlet/exit thickness | 1.6/1.152mm |
| Roller radius | 100mm |
| Back/front tension stress | 65/75MPa |
| Young’s Modulus (strip) | 210GPa |
| Poisson’s ratio (strip) | 0.3 |
| Tresca yield stress | 230+1200* ε |
| Coulomb friction coefficient | 0.08(bite-in),0.075(quasi-static) |
| Strip width | 200mm |
| Roller crown | 5 μ m |

First, the comparison between SM and FEM (Abaqus® implicit, quasi-static 2D) is presented for the elastic-plastic strip deformation. Top/bottom symmetry has been assumed, rolls are rigid. With about 50x5 CPS4R elements and a time step of 2e-4 second in the roll bite, FE convergence has been reached. To deal with the engagement of the strip in the roll bite, a three-step strategy has been used with the FEM: first, setting a firm contact, then bite-in with a higher friction coefficient whereas roll accelerates, finally reaching a quasi-steady rolling process with parameters of table 1.

The SM calculation costs only a few seconds whereas tens of minutes are needed for FEM to reach a quasi-steady state. Fig .1 (a) shows that there is a shear effect at bite entry, as seen by the non-strictly vertical contour lines of the strain; it could be evidenced by plotting the strain rate map with an adapted (logarithmic) scale, but this is not done here due to the small impact of this feature. This point is indeed marked by a slight normal pressure peak in the

FEM results, but again it does not impair the good agreement of the global profiles (Fig. 1 (b)). Furthermore, this effect would further reduce if thinner strips (higher bite length / thickness ratio [4]) were simulated such as in last passes of cold tandem mill, in double reduction or even in foil rolling, where the major problems arise.

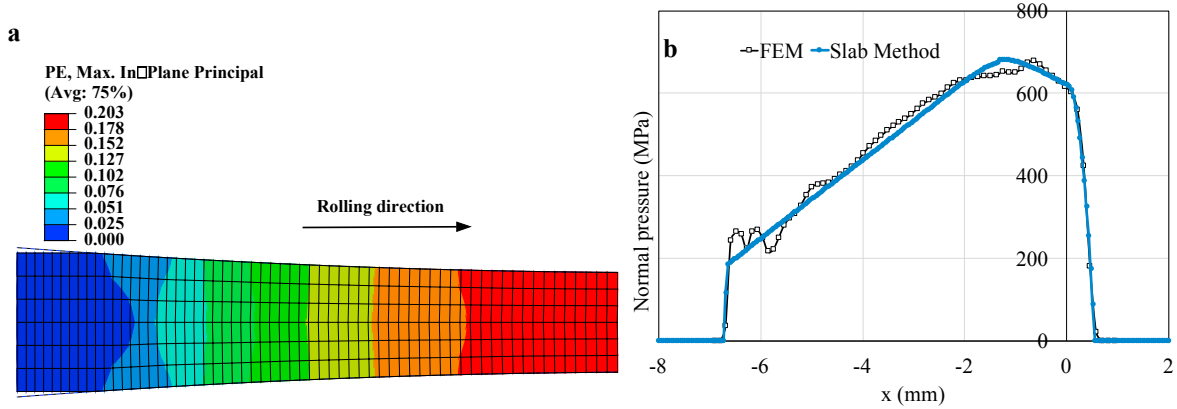


Fig. 1. 2D strip deformation models comparison, SM vs FEM. (a) equivalent plastic strain; (b) normal pressure

3.2. 3D Case: discussion of the plane strain assumption

From the above 2D case, a 3D case was built with the same, uniform back/front tensions assumed across the transverse (y) direction. Constitutive models are isotropic, i.e. friction in the y direction is the same as in x direction. A rigid work roll with a 5 μm quadratic crown is used to bring a concave shape change

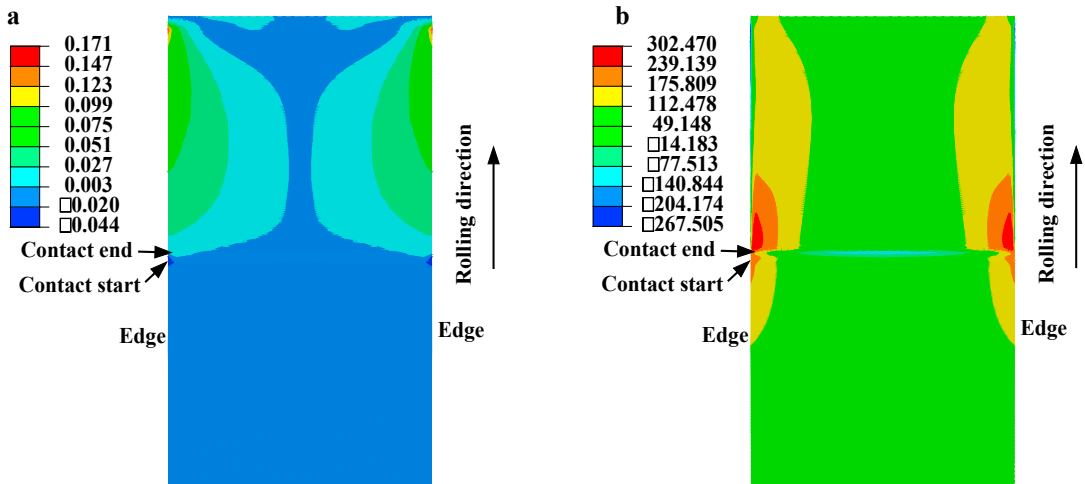


Fig. 2. Top view of the rolled strip during 3D FEM modelling. (a) y-displacement in the strip; (b) stress map $\sigma_{xx}(x,y)$

Fig. 2 (a) confirms that under the abovementioned assumptions, the lateral flow is present but small – spread is about 0.08mm in the steady state, to be compared with half strip width 100mm. This fundamental assumption of the multi-slab model is therefore validated. On the other hand, Fig.2 (b) shows that $\sigma_{xx}(y)$ varies significantly; on either sides of the roll bite (but with more intensity at exit), a strong tension is induced in the edges which are less deformed due to the roll crown – and therefore tend to have a lower forward velocity. Note that steady state has not been reached exactly, which would require rolling a length of approximately twice the strip width, i.e. 400 mm.

3.3. 4/6 high roll stack modelling: 3D FEM vs IFM.

The FE model has been set up to study the elastic deformation of a 6-high roll stack with IR shifting. Parameters are given in Table 2. Bending forces of 46kN and 200kN have been applied on work rolls and intermediate rolls respectively to counter-bend WR under an assumed uniform rolling load of 8kN/mm (the strip deformation is not modelled in this section). The mesh is refined at the roll/roll contact areas, see Fig.3 (a) and (b). Nodal contact forces from FEM have been reprocessed into a contact line load, in order to be compared with IFM.

Table 2. Parameters used for the elastic deformation of the rollers

| Variables | Value |
|------------------------------------|--------|
| Work roll (WR) diameter | 425mm |
| Work roll barrel length | 1500mm |
| Work roll bending position | 915mm |
| Intermediate roll (IMR) diameter | 490mm |
| Intermediate roll barrel length | 1510mm |
| Intermediate roll shifting | 93.2mm |
| Intermediate roll bending position | 905mm |
| Back up roll (BUR) diameter | 1300mm |
| Back up roll barrel length | 1510m |
| Screw down position | 905mm |

Fig. 3 (c) shows that the IFM roll stack elastic deformation model has a great precision at a low cost. It took 6 to 12 Newton-Raphson's iterations to achieve convergence (remember that the roll stack model is non-linear due to evolving roll/roll contact); the total cost is a few seconds, while the load difference with FEM is negligible.

4. Conclusion

Current progress of developing mathematical model with better cost/quality ratio for cold rolling strip process has been reported in the present paper. It revisits the model of Pawelski [6], which took advantage of the engineering feature of cold rolling that the reduction in thickness only results in elongation in rolling direction (lateral spread is very small). Progress has been made by incorporating an elastic-plastic Slab Method and an Influence Function Method for 4/6-high roll stack compilation with Hacquin's correction.

The advantage and limitations of the developed model have been discussed. It is shown that the present model matches FEM results at a lower computational cost, in terms of strip deformation (SM predicting local roll load) and the transmission of contact loads through the roll stack. A good precision can therefore be expected on the prediction of strip crown (transverse thickness profile). What is neglected is the intrinsically 3D problem of strip lateral widening/shrinking, which is important in itself (for width tolerance control) and may also impact very locally the load distribution near the edge and the edge-drop defect; flatness of course cannot be directly addressed, it needs to be processed by a different model from a comparison of entry and exit strip crowns.

It should be pointed out that there are few experimental results on the contact mechanics of cold strip rolling in the transverse direction; also the question of friction anisotropy and its potential consequences remains open. Further efforts by the authors to achieve a fully coupled iterative model will be reported in future papers.

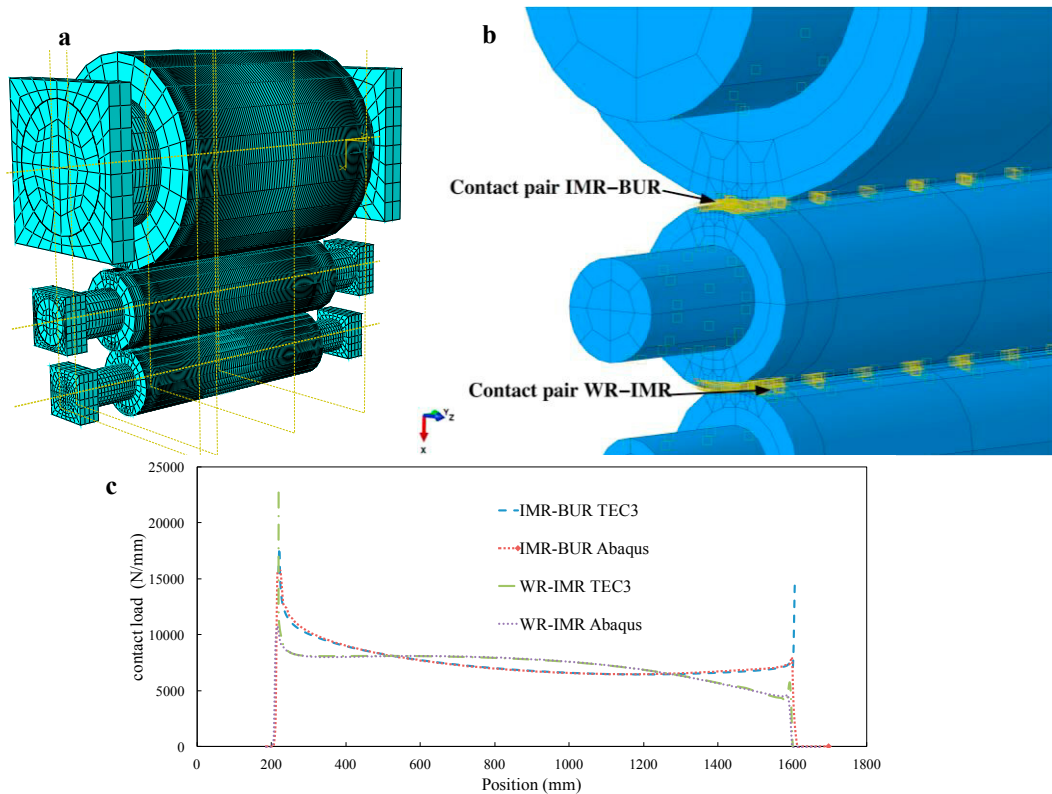


Fig.3. Checking roll stack model. (a) the FEM mesh; (b) focus on the edges of contacts where mesh is refined; (c) FEM / IFM comparison of roll – roll contact loads

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