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# Experimental-Numerical Validation Framework for Micromechanical Simulations

Ante Buljac, Modesar Shakoor, Jan Neggers, Marc Bernacki,  
Pierre-Olivier Bouchard, Lukas Helfen, Thilo F. Morgeneyer, and François Hild

**Abstract** A combined experimental-numerical framework is presented in order to validate computations at the microscale. It is illustrated for a flat specimen with two holes, which is made of cast iron and imaged via *in situ* synchrotron laminography at micrometer resolution during a tensile test. The region in the reconstructed volume between the two holes is analyzed via Digital Volume Correlation (DVC) to measure displacement fields. Finite Element (FE) simulations, whose mesh is made consistent with the studied material microstructure, are driven by measured Dirichlet boundary conditions. Damage levels and gray level residuals for DVC measurements *and* FE simulations are assessed for validation purposes.

## 1 Introduction

The prediction of forming processes and in-service life of metals and alloys raises important issues for ductile fracture, which have led researchers to investigate ad-

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vanced damage models. A first type of damage models, which is known as macroscopic postulates [1, 2, 3], is used to predict not only damage inception but also the softening and transition to fracture. Due to their macroscopic nature, they are known to have limited predictive capabilities and are usually calibrated and applied for specific loading conditions. For applications such as material forming, where loading may be complex and non proportional, these limitations become problematic [4, 5].

Microscopic models [6, 7] are an alternative where the macroscopic response is derived from averaged microscale calculations. This scale transition may be purely analytical [6] or performed via computations on ideal microstructures [7]. The predictive capacities of such models are also limited for arbitrary loading conditions [4, 5] because of restrictive assumptions used in their derivations [6, 7]. Further, the calibration of these models is challenging since they usually require advanced identification techniques [8, 9, 10]. It is worth noting that some damage variables such as porosity can now be observed experimentally thanks to X-ray imaging techniques [11, 12, 13, 14]. Inclusions and voids can be studied individually based on manual [13, 15] or automatic [14] procedures.

Simulations allow experimentally observed quantities such as porosity and number of fractured/debonded inclusions to be related to internal variables such as plastic strain and stress-based criteria. These microscale computations are usually driven with idealistic microstructures, constitutive behavior, and simplified kinematic or static boundary conditions that do not capture local strain and stress states that inclusions and voids are subjected to [11, 16, 17, 14]. The principal aim of the present work is to develop reliable simulations at the microscale using validated models to describe the three steps of ductile damage (*i.e.*, nucleation, growth and coalescence). The first step then consists of developing an experimental-numerical framework, which enables numerical models to be probed with respect to experimental data.

The material of interest is nodular graphite cast iron made of a ferritic matrix, graphite nodules, and no significant initial porosity. Upon loading, ductile fracture is caused by nodule/matrix debonding, void growth and coalescence [18, 19, 20]. Literature data [18, 21, 22, 19] show that the nodules can be modeled as voids since their stress-carrying capacity is very small in tension. Such hypothesis will be made herein. One of the present challenges is to test this type of assumption with local error estimators (*i.e.*, at the microscale). It will also allow microscopic models to be developed in order to better capture the final stages of failure via calibrated criteria associated with different mechanisms [23, 24].

The framework followed herein, which was first applied to another test case [25], quantitatively compares experimental bulk data with 3D computations. It consists of the following steps (Figure 1):

- X-ray laminography, which is a non-destructive 3D imaging technique for laterally extended 3D objects [26, 27, 28, 29, 30], to acquire radiographs and subsequently reconstruct 3D volumes of different steps of a mechanical test. By post-processing such bulk data, the morphology of the two-phase microstructure can be revealed and its changes can be analyzed.
- Digital volume correlation (DVC) to measure 3D displacement fields [31, 32, 33, 34]. Small interrogation volumes are *independently* registered in the considered

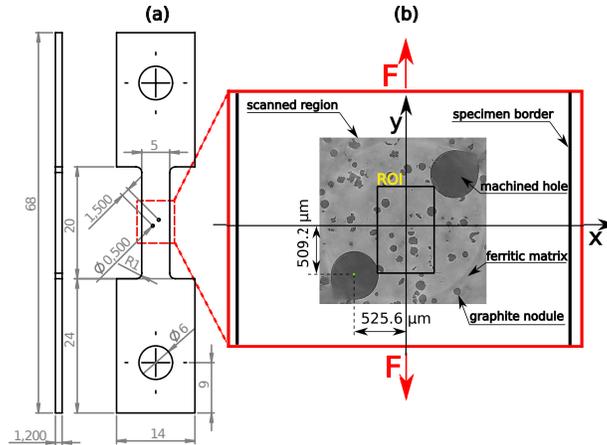


The chapter is structured as follows. The experimental setup and laminography are first discussed. Digital Volume Correlation is summarized next. Uncertainty quantifications are performed. FE computations including the microstructure meshing procedure are then described. Last, the results from both methods are compared relatively via kinematic field subtractions and absolutely by computing gray level residuals. The predictions of the damage state are also confronted with experimental evidence.

## 2 Experimental and numerical framework

### 2.1 Experiments

The studied material is commercial nodular graphite cast iron (serial code: EN-GJS-400). Figure 2(a) shows the sample geometry, which is inspired by Ref. [48]. The holes have been machined via Electrical Discharge Machining (EDM). The load is manually applied to the sample by controlling the global relative displacement via screw rotation.

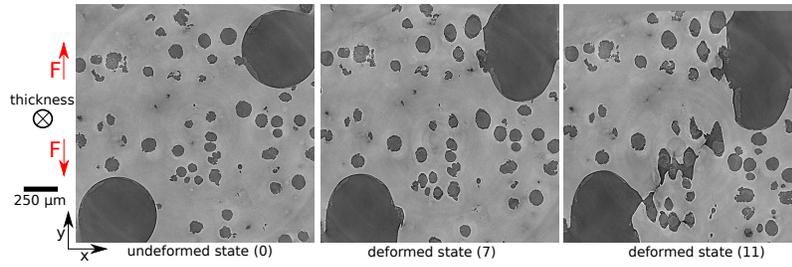


**Fig. 2** (a) Sample geometry with the scanned region between pin holes; (b) section of the reconstructed volume with ROI position

After applying each loading step, a set of radiographs is acquired while the sample is rotated about the laminographic axis (*i.e.*, parallel to the specimen thickness direction). This axis is inclined with respect to the X-ray beam direction by an angle  $\theta \approx 60^\circ$ . The series of radiographs is then used to reconstruct 3D volumes via filtered-back projection [49]. A GPU-accelerated implementation of this algorithm [50] has been utilized herein. The reconstructed volume size is

$1600 \times 1600 \times 1600$  voxels (each voxel has a physical length of  $1.1 \mu\text{m}$ ). After scanning the undeformed state (0) three times, 12 additional scans are performed upon stepwise loading. The last scan corresponds to the final crack.

The scanned zone encompasses the two holes. The selected ROI for DVC *and* FE calculations mainly focuses on the ligament between the two holes (Figure 2(b)). The two machined holes are  $500 \mu\text{m}$  in diameter and the nodule population, which is assumed to behave as voids in the FE computations, has a characteristic diameter of  $60 \mu\text{m}$ . It is considered as secondary void population, which can be observed at micrometer resolutions. Figure 3 shows mid-thickness sections of the reconstructed volume for three different load stages. Classical void coalescence mechanisms are accompanied by sheet coalescence between the two machined holes in the last loading step (deformed state (11)).



**Fig. 3** Mid-thickness section of the reconstructed volume for three different loading steps

## 2.2 Digital Volume Correlation

Global DVC, which is used herein, is an extension of global 2D DIC [51, 52]. Reconstructed volumes are described by discrete gray level fields of spatial (voxel) coordinate  $\mathbf{x}$ . DVC consists in registering the gray levels  $I_0$  in the reference configuration with those of the deformed volume  $I_t$  such that their conservation is obtained

$$I_0(\mathbf{x}) = I_t[\mathbf{x} + \mathbf{u}(\mathbf{x})] \quad (1)$$

where  $\mathbf{u}$  is the Lagrangian displacement field. In experiments gray level conservation (1) is never satisfied in laminography due to acquisition noise and reconstruction artifacts [53]. Therefore the gray level residual  $\rho(\mathbf{x}) = I_0(\mathbf{x}) - I_t[\mathbf{x} + \mathbf{u}(\mathbf{x})]$  is globally minimized by considering its L2-norm with respect to kinematic unknowns, which parameterize the measured displacement field. For global DVC, the whole ROI is considered and the global residual  $\Phi_c^2$

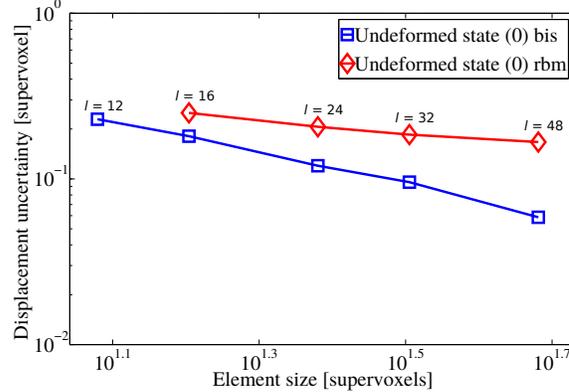
$$\Phi_c^2(\{\mathbf{u}\}) = \sum_{ROI} \rho^2(\mathbf{x}, \{\mathbf{u}\}) \quad (2)$$

is minimized with respect to the unknown degrees of freedom  $u_p$  gathered in the column vector  $\{\mathbf{u}\}$  when the displacement field is written as

$$\mathbf{u}(\mathbf{x}, \{\mathbf{u}\}) = \sum_p u_p \Psi_p(\mathbf{x}) \quad (3)$$

where  $\Psi_p(\mathbf{x})$  are selected displacement fields associated with the parameterization of  $\mathbf{u}(\mathbf{x}, \{\mathbf{u}\})$ . Finite element shape functions are of particular interest since they provide direct links between measured displacement fields and numerical simulations. DVC based on hexahedral finite elements with trilinear shape functions [35] is utilized herein. Only a part of the reconstructed volume, which is referred to as DVC ROI, is considered (Figure 2(b)). To keep large ROI sizes, the reconstructed volumes are coarsened (*i.e.*, each 8 neighboring voxels are averaged to form one supervoxel).

The measurement uncertainties are quantified by registering two volumes of the unloaded sample (0) with (coined “rbm”) and without (*i.e.*, “bis”) rigid body motion (RBM) applied between acquisitions. Noise and reconstruction artifacts make these two volumes non identical. The corresponding displacement fields account for laminography and DVC effects on the measurement uncertainties [54]. The measurement uncertainties are assessed by the standard deviation of displacement fields. Figure 4 shows the standard displacement uncertainties for different element sizes  $\ell$ . Decreasing the element size induces an increase of the displacement uncertainty [55, 56]. The element size used hereafter is set to  $\ell = 16$  supervoxels and corresponds to a standard displacement uncertainty of 0.25 supervoxel. This level is the limit below which the estimated displacement levels are no longer trustworthy.



**Fig. 4** Standard displacement uncertainties as functions of the element size  $\ell$  expressed in supervoxels for two different acquisitions of the reference configuration

Successful DVC registrations were achieved for the first 9 incremental calculations (*i.e.*, registrations between step  $n - 1$  and step  $n$ ). The measured displacement

fields will serve as DVC-FE boundary conditions. The measured displacement fields are interpolated for each loading step onto the FE mesh of the ROI using the shape functions of the DVC mesh).

### 2.3 Simulations

To perform microscale FE simulations the numerical framework discussed in Refs. [44, 57, 46, 58, 47] is followed. The ROI selected for the FE simulations has to belong to all DVC ROIs for each analyzed loading step and to be made as large as possible [25]. To model the experimental microstructure standard image processing operations are carried out [59, 60], namely, smoothing the data, applying a gray value threshold to separate matrix and voids, and then converting these binary data into signed distance function. The latter is interpolated onto a first mesh of uniform size of  $10 \mu\text{m}$  of the FE ROI via trilinear interpolation. The corresponding signed distance function is then regularized with a parallel reinitialization algorithm [46], and used to locate the interfaces [25, 47]. An adaption step is added to control the local maximum curvature of the interface [25, 58]. These different steps are exemplified in Figure 5 for a 2D laminography section. The final mesh has a size of  $10 \mu\text{m}$  close to matrix/void interfaces and  $50 \mu\text{m}$  at a distance of  $100 \mu\text{m}$  from any interface with a linear transition. As shown in Figure 5 the FE discretization of the microstructure is very close to the experimental observation.

The graphite nodules are modeled as zones with very low Young's modulus [18, 21, 22, 19, 25], while the ferritic matrix is considered as an elastoplastic medium with power law hardening

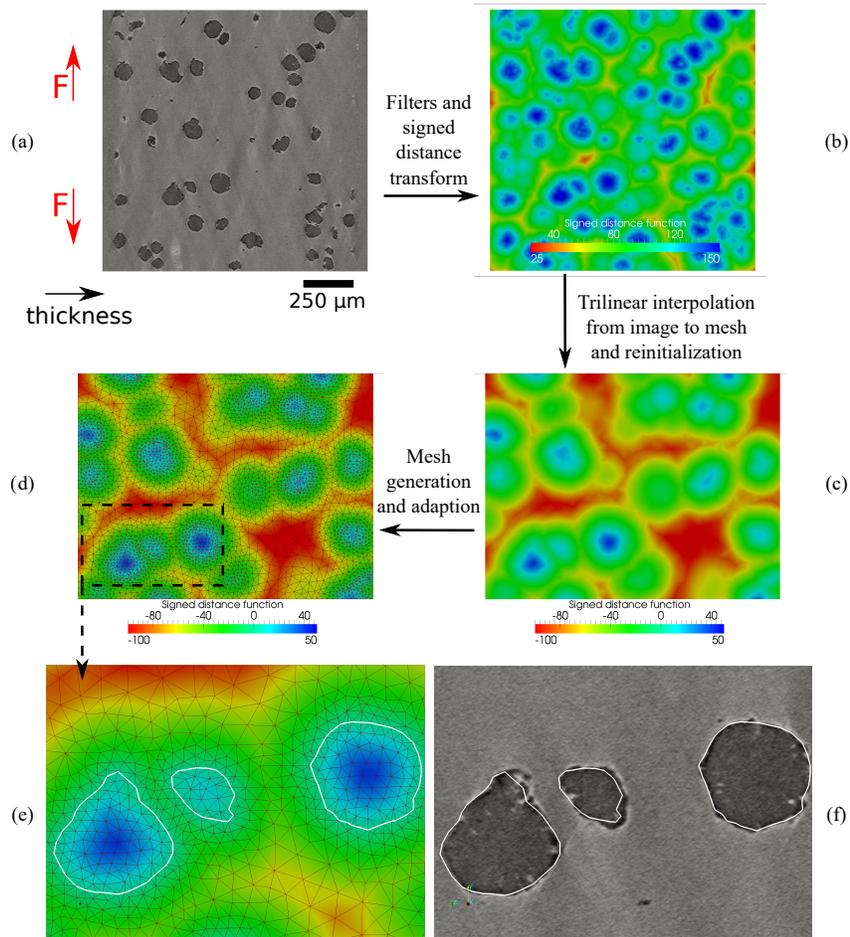
$$\sigma_0(p) = \sigma_y + Kp^n \quad (4)$$

where  $p$  is the equivalent plastic strain,  $\sigma_y$  the initial yield stress,  $K$  the plastic modulus and  $n$  the hardening exponent. The properties of the matrix (Table 1) are deduced from tensile experiments on pure ferrite [21].

**Table 1** Elastoplastic properties of the ferritic matrix

$E$ (GPa)	$\nu$	$\sigma_y$ (MPa)	$K$ (MPa)	$n$
210	0.30	290	382	0.35

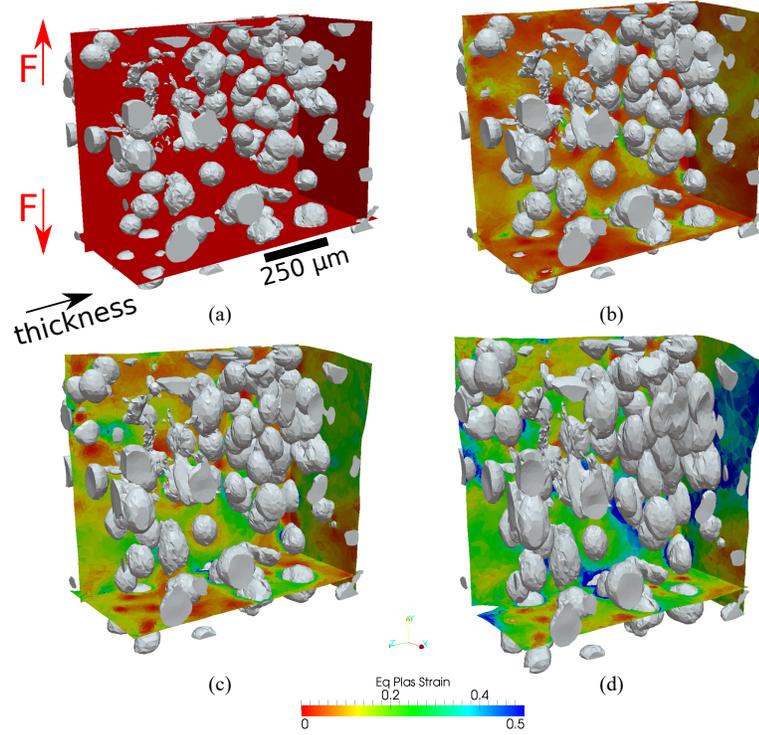
The satisfaction of equilibrium equations is obtained with a mixed velocity-pressure formulation solved with  $P1^+/P1$  elements to avoid locking [61]. The non-linear behavior of the matrix requires Newton-Raphson schemes to be implemented locally and globally [62]. An updated Lagrangian scheme is used to handle large deformations. Further, large distortions and possible flip of elements are avoided with automatic mesh motion and adaption [47].



**Fig. 5** Image immersion and meshing. (a) Initial laminography 2D section. (b) Signed distance function computed thanks to image processing. (c) Signed distance function interpolated and reinitialized on the FE mesh [46]. (d) Conforming FE mesh generated and adapted to interfaces and local maximum curvature, (e) Zoom on the FE mesh. (f) Comparison between initial laminography 2D section and interfaces in the final FE mesh (in white)

### 3 Results

The numerical results using DVC-FE are illustrated in Figure 6. This computation considers 100 voids meshed with  $\approx 1$  million elements. Void growth and equivalent plastic strains develop as more load is applied.



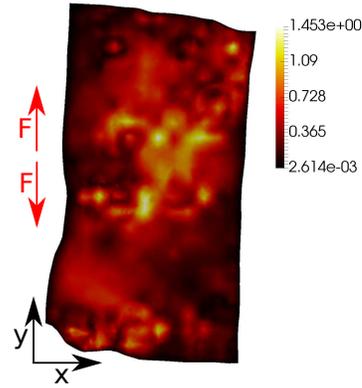
**Fig. 6** ROI calculation results using DVC-FE showing the 3D meshed voids and the equivalent plastic strain on sections when: (a)  $u = 0$  (undeformed state), (b)  $u = 83.4 \mu\text{m}$ , (c)  $u = 192.2 \mu\text{m}$ , (d)  $u = 320.8 \mu\text{m}$

### 3.1 Error estimators

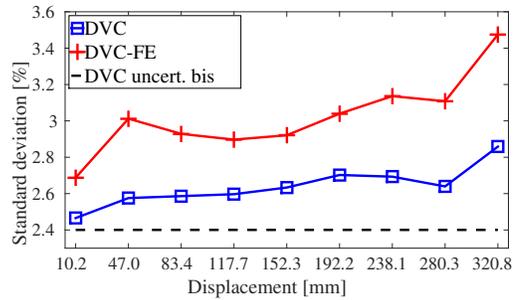
Relative displacement comparisons are first reported. Measured displacement fields (via DVC) are applied to the boundaries of the FE ROI. They are also available within the whole ROI. Thus, DVC and DVC-FE displacement fields can be interpolated on the same mesh and directly compared as reported in Figure 7. The main differences are concentrated around debond zones between the matrix and the nodules, while those close to the boundaries are mostly zero. The fact that the differences become significantly larger than the displacement uncertainty is a first indication of model error.

The errors in terms of gray level residuals are now discussed. For each pair of consecutive loading steps, the volume reconstructed for the second step can be deformed back with the measured or computed displacement field. This corrected volume can be compared *voxelwise* with the volume of the first step. With a newly developed tetrahedral-DVC code [63, 38] FE computations with tetrahedral meshes can be imported in the reconstructed volumes frame where the displacement fields

**Fig. 7** Mid-section normal to  $z$ -direction showing absolute difference between DVC and DVC-FE displacement fields. The displacement difference is expressed in supervoxels (1 supervoxel  $\longleftrightarrow 2.2 \mu\text{m}$ )

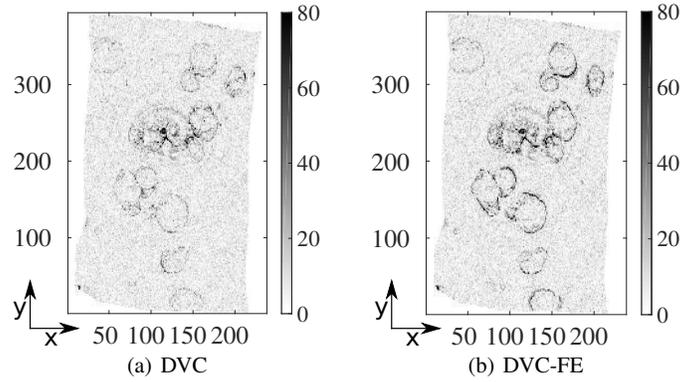


are interpolated voxelwise. The deformed volume  $I_t(\mathbf{x})$  is corrected by the computed displacement field  $\mathbf{u}_{FE}(\mathbf{x})$ , *i.e.*,  $I_t(\mathbf{x} + \mathbf{u}_{FE}(\mathbf{x}))$  is obtained. The gray level residuals, namely, differences between the volume of the reference configuration  $I_0(\mathbf{x})$  and the corrected deformed volume  $I_t(\mathbf{x} + \mathbf{u}(\mathbf{x}))$  are assessed for DVC and FE computations. Quantitative and local error measurements are evaluated for DVC and DVC-FE procedures. Figure 8 shows the standard deviation of residual fields that are normalized by the dynamic range of the volume (*i.e.*, 256 gray levels). The DVC residuals remain close to those observed in the uncertainty analysis for which no strains occurred. Therefore the DVC results are deemed trustworthy.



**Fig. 8** Standard deviation for the dimensionless gray level residual fields for all loading steps. For comparison purposes, the dashed line corresponds to the uncertainty analysis for the so-called “bis” case (see Subsection 2.2)

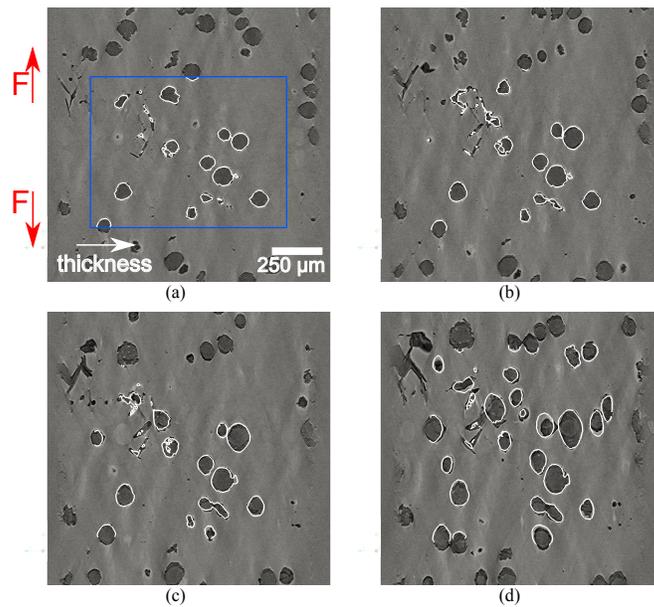
The errors produced by the micromechanical models inside the DVC-FE domain also remain low and slightly increase at later loading steps (from  $\approx 15\%$  initially to  $\approx 20\%$  in last loading step). However they are always higher than the DVC residuals. This observation confirms model errors that become more significant as coalescence sets in. Figure 9 confirms that these differences between DVC-FE simulations and experiments are mostly concentrated around interfaces.



**Fig. 9** Absolute gray level differences at the  $z$  midsection after correction with DVC (a) and DVC-FE (b) displacements for the ninth loading step

### 3.2 Damage analysis

Damage predictions of DVC-FE are qualitatively compared studying the  $x$ -midsection of the ROI with experimental images in Figure 10. Since measured boundary condi-

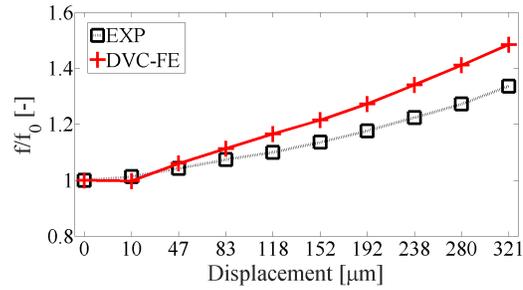


**Fig. 10** ROI (blue line) calculation results using DVC-FE comparing the numerical matrix/void interface (white line) with experimental images for the  $x$ -midsection. (a)  $u = 0$  (undeformed state), (b)  $u = 83.4 \mu\text{m}$ , (c)  $u = 192.2 \mu\text{m}$ , (d)  $u = 320.8 \mu\text{m}$

tions are expected to follow experimental images at the spatial resolution of DVC, the matrix/void interfaces in the simulation (in white in the figure) are superimposed. The interfaces are very accurately meshed on average and tracked during the simulation up to the last loading step. Quantitatively void growth is defined by

$$f = \frac{\text{void volume}}{\text{ROI volume}} \quad , \quad \text{void growth} = \frac{f}{f_0} \quad (5)$$

where  $f_0$  is the initial void volume fraction. Void growth plots are shown in Figure 11 in which the ‘EXP’ curve is obtained in processed laminography volumes (*i.e.*, images with smooth signed distance functions as shown in Figure 5(b)).



**Fig. 11** Void volume change observed experimentally and predicted within the present framework

The numerical results show a small decrease of porosity  $p$  at the first loading step. This is not observed experimentally. This first loading step is bigger than the subsequent ones, which asks for extensive remeshing in the computations. Consequently interfaces are slightly smoothed and void volume can be diffused. For the other loading steps, void growth is overestimated numerically. This may be due to the fact that nodules are considered as very soft media in the computations, while in reality only the voids grow after nodule/matrix interface debonding (Figure 10).

## 4 Discussion

Although the results using DVC-FE look very promising, several issues need to be addressed. There still are gaps between FE-DVC and DVC results (see Figures 9 and 10). This gap increases when reaching the final loading steps. Similarly, the displacement difference (Figure 7) is significantly higher than the displacement uncertainty reported in Figure 4. The differences are mainly concentrated around matrix/nodule interfaces. This observation calls for better models of the nodules and interface debonding. Further, the increase of the error at later loading steps proves the inability of the constitutive law used for the ferritic matrix to fully capture the acceleration of void growth and subsequent coalescence. Better calibrated and more

advanced plasticity models may be considered at the microscale to better capture the multiscale plastic flow. These additional developments will extensively rely on DVC-FE and its ability to provide experimentally measured boundary conditions for micromechanical simulations. The extension of Integrated-DVC to 4D analyses [38] will be utilized to conduct inverse analyses based on these error measurements and calibrate material parameters at the microscale.

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